



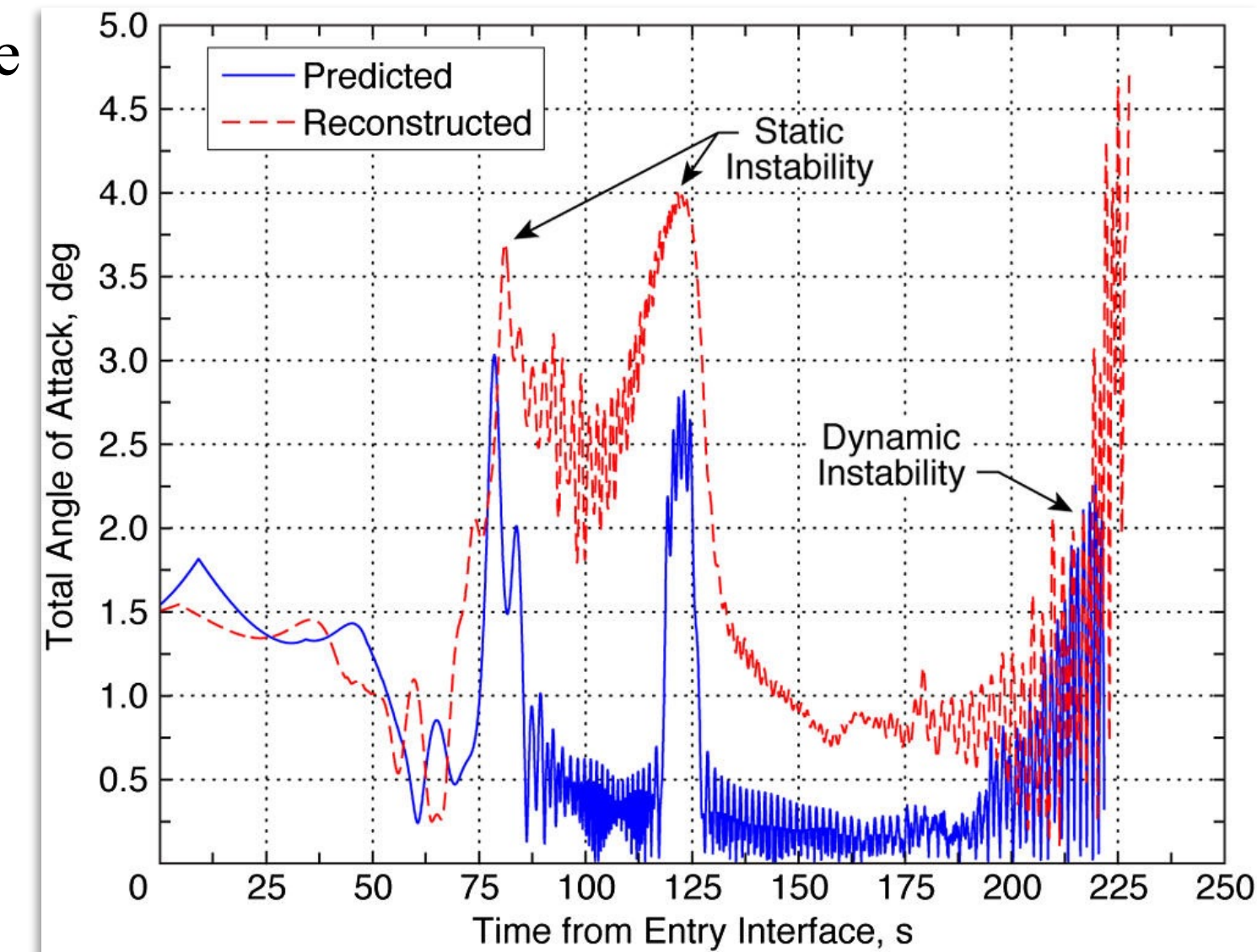
Dynamic Stability Methodologies and Capabilities

Joseph Brock
Eric Stern
Cole Kazemba
Quincy McKown
Dirk Ekelschot

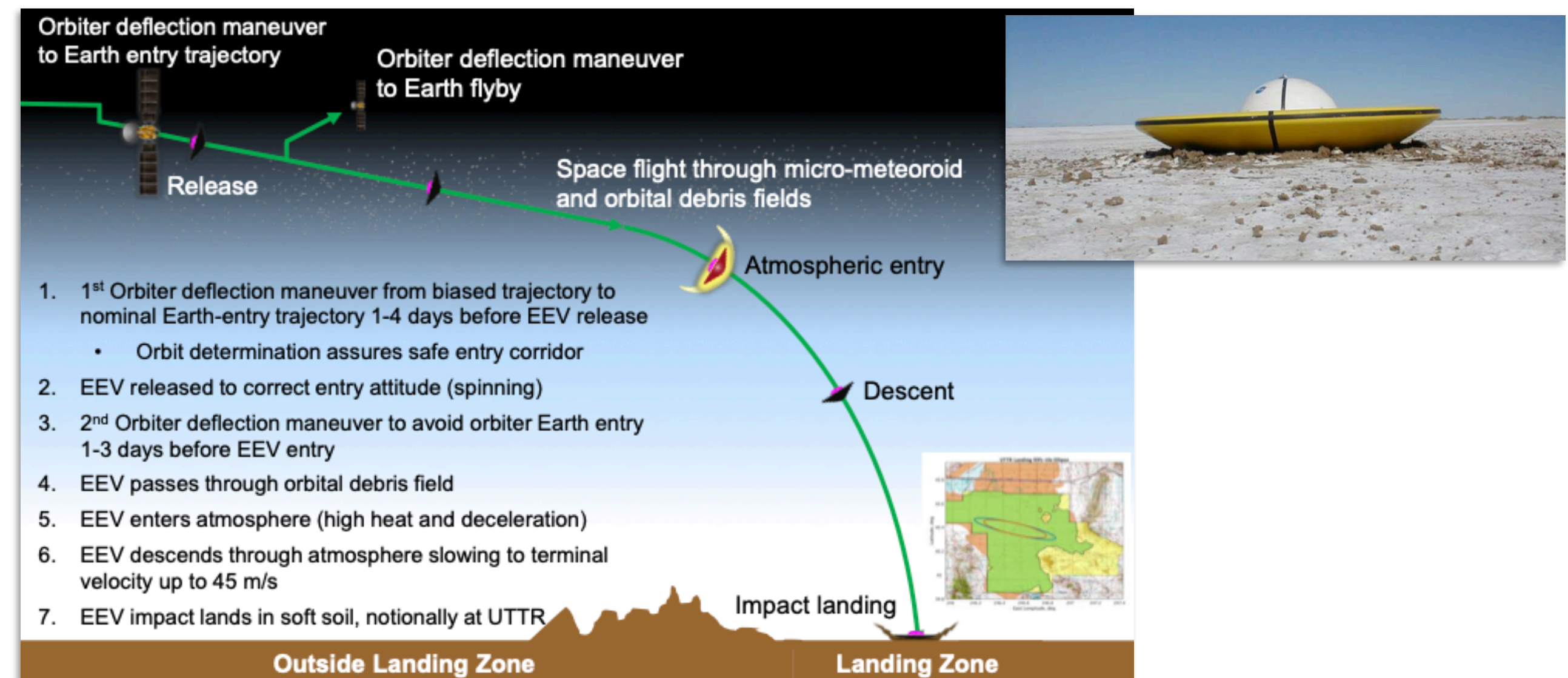
Characterization of Dynamic Stability

- Blunt-body capsules are subject to dynamic instabilities at low-supersonic and transonic Mach numbers
- Dynamic stability typically characterized exclusively via experiment: forced-, free-oscillation, and ballistic range
 - These methods have a long pedigree of producing dynamic aero for missions
 - However, each method has drawbacks resulting in uncertain predictions
- Current entry missions have dynamics challenges:
 - MSR EES: dynamics during terminal descent drive impact angle which is key for containment
 - Dragonfly: coupled capsule-chute dynamics drive Lander separation event
- Mission needs motivate improved capabilities beyond what standard methods can provide
- Renewed effort on various fronts to characterize dynamics via new testing and computational methods

Mars Phoenix Lander (Desai, 2011)



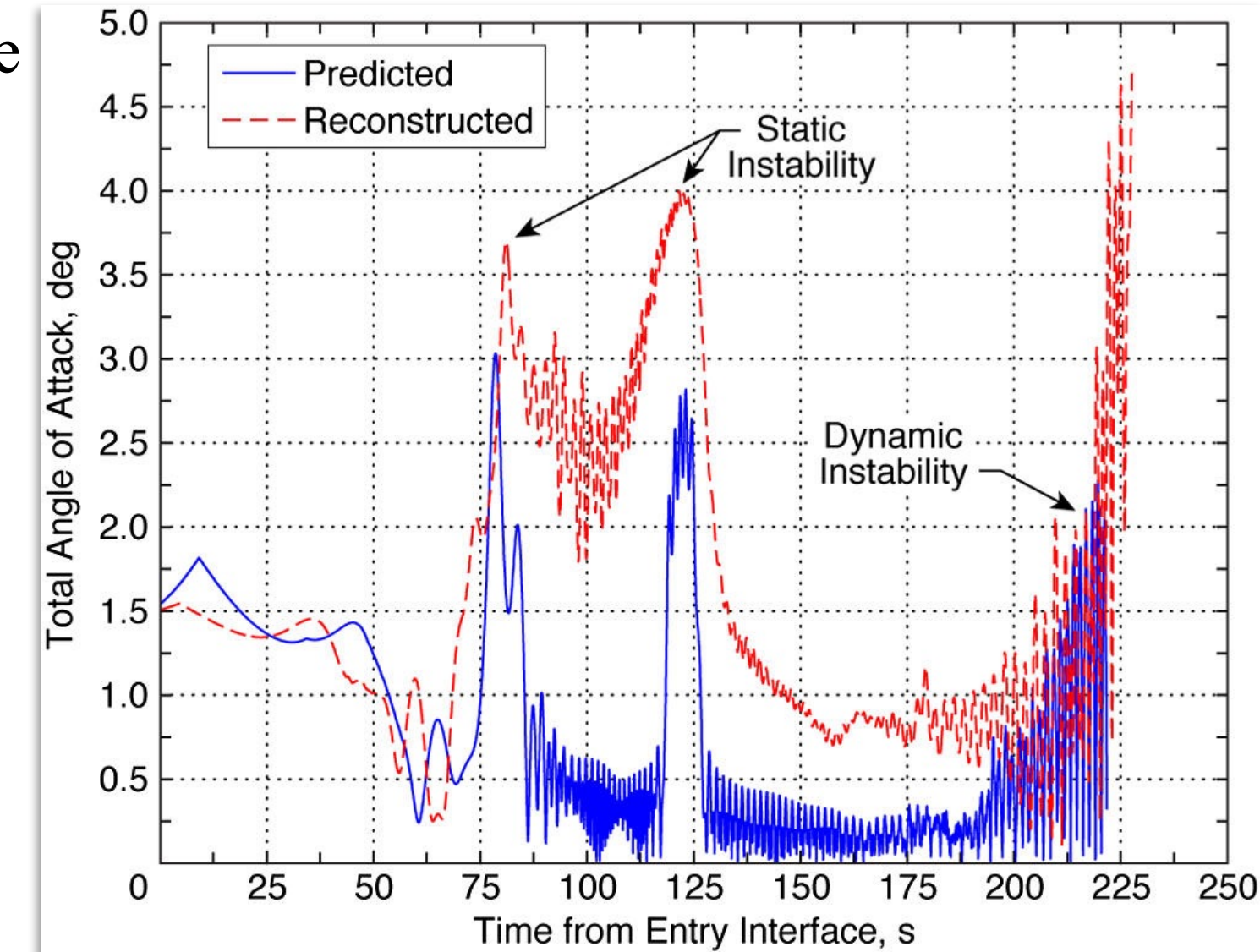
Dynamic instabilities of blunt bodies often arise at low-supersonic and transonic Mach numbers



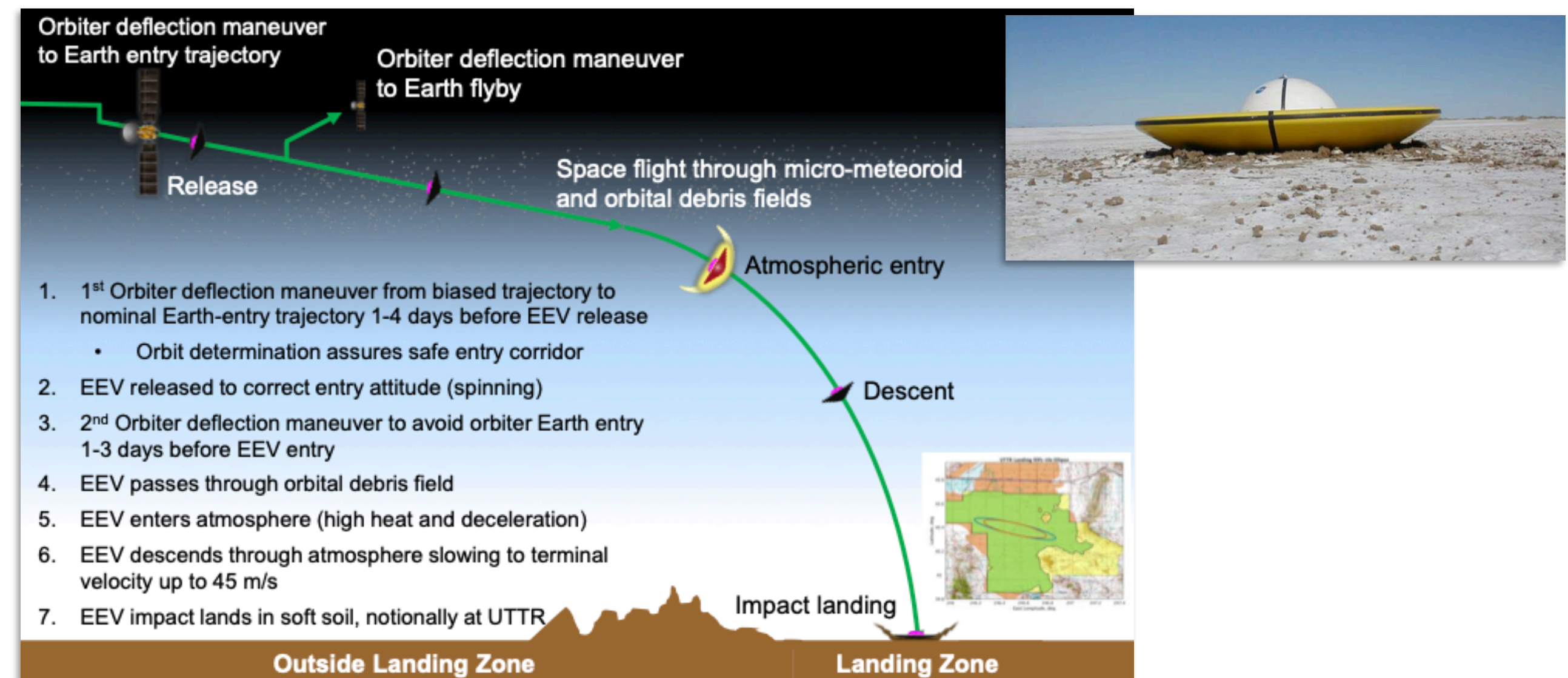
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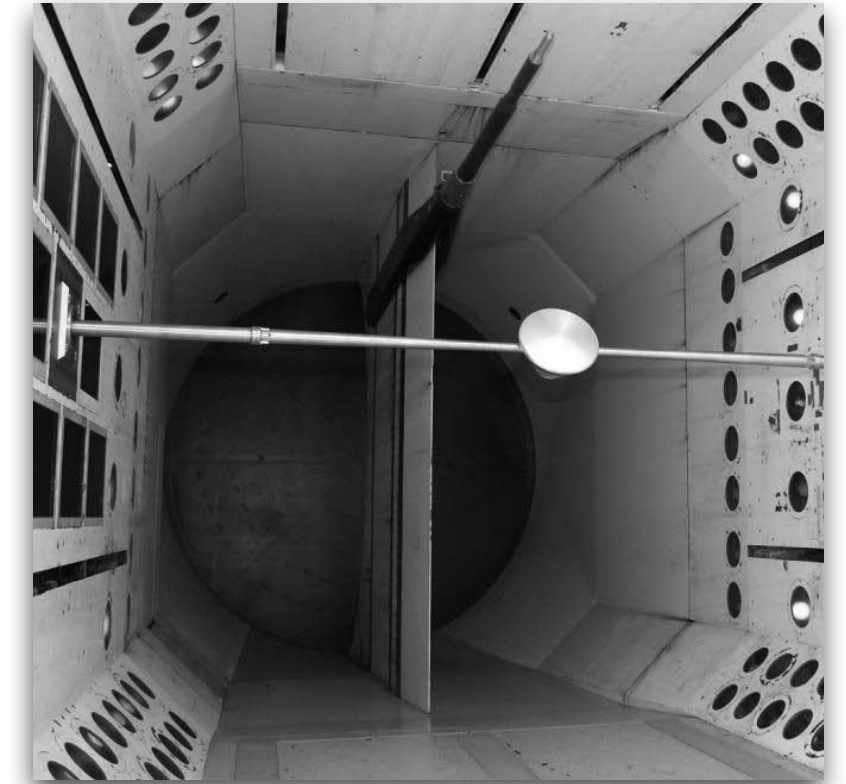
State of the Art: Experimental Facilities

- The current paradigm for dynamic stability testing relies on a piecemeal of different test methods:
 - Multiple test methods provides Mach coverage and helps to compensate for the deficiencies of each individual test method.
 - Flight testing requires typically occurs at lower speeds, sub-scale, or approximate Reynolds number due to gas composition differences
 - Sting mounted setups mirror classic wind-tunnel approaches to provide force and moment data directly
 - Each test methodology relies on a different data reduction approach, all of which differ from flight reconstruction methods
 - Little overlap between the attainable Mach numbers for the different methodologies.
- Each test approach has one or more key weaknesses:
 - Facility induced effects (e.g. stings)
 - Ability to match dynamic similitude and/or Reynolds Number
 - Richness of data for reconstruction and ADB development (e.g. loss of forces/moment data)
- Number of available test facilities is limited:
 - NASA Ames HFFAF and Aberdeen are the only available ballistic range facilities
 - NASA LaRC TDT facility is standard for free- and forced oscillation. Scheduling is difficult
 - Subsonic MWST is coming online to address some of the weakness above

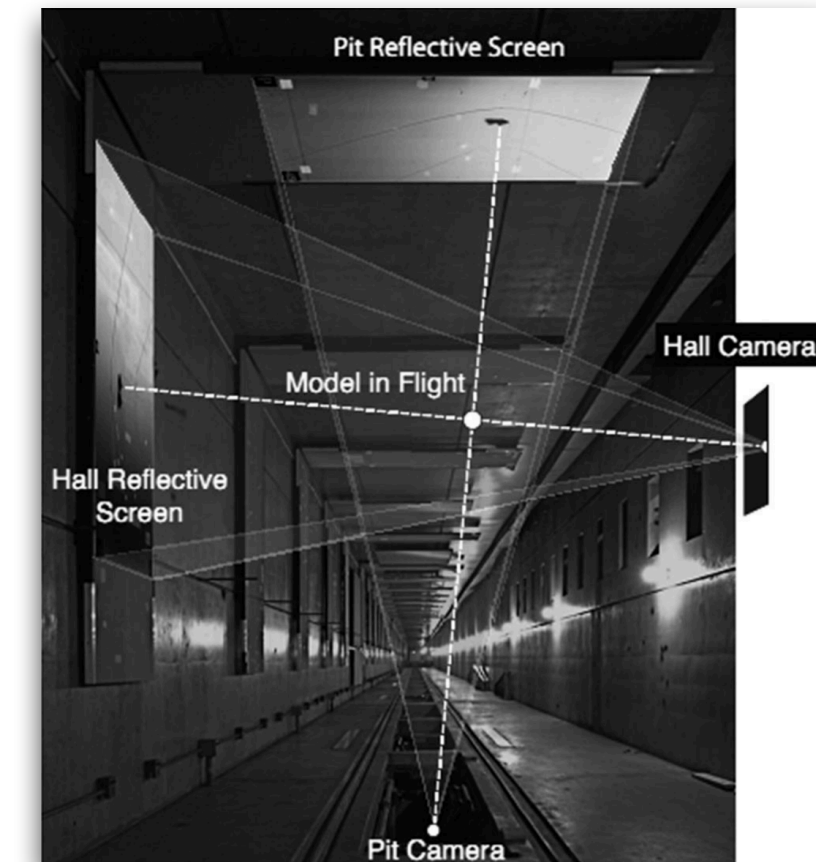
Vertical Spin Tunnel (VST)



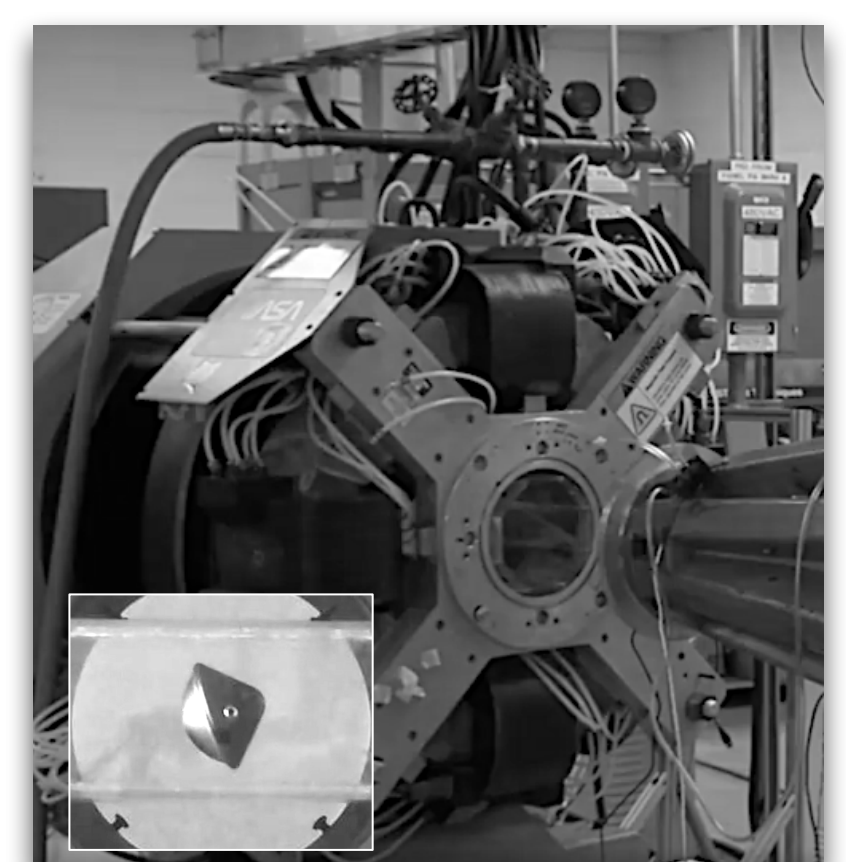
Transonic Dynamics Tunnel (TDT)



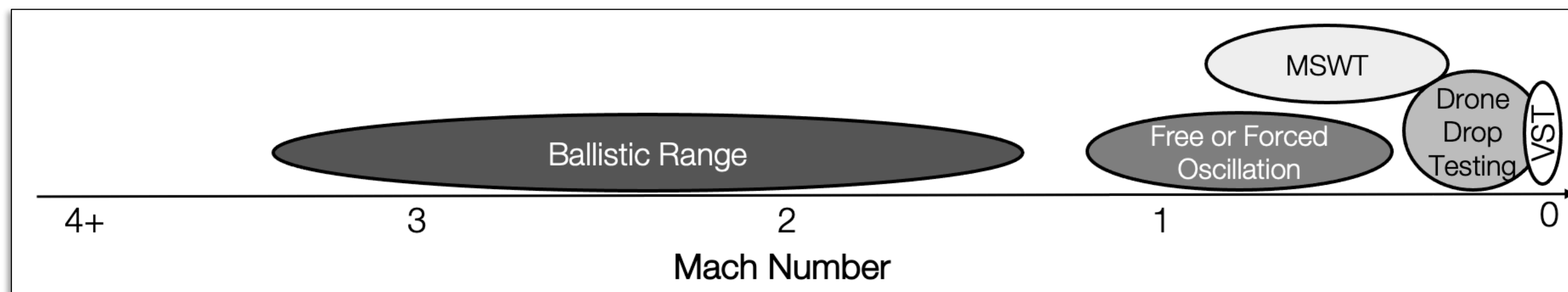
Indoor Ballistic Range



Magnetic Suspension Wind Tunnel



Hypervelocity Free Flight Aerodynamics Facility (HFFAF)



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 - Flight testing requires typically occurs at lower speeds, sub-scale, or approximate Reynolds number due to gas composition differences
 - Sting mounted setups mirror classic wind-tunnel approaches to provide force and moment data directly
 - Each test method provides a different level of detail in the reconstruction
 - Little overlap between methods

- Each test approach has its own strengths and weaknesses:
 - Facility induced noise
 - Ability to match flight conditions
 - Richness of data

- Number of available facilities:
 - NASA Ames HST
 - NASA LaRC T
 - Subsonic MWS

There is no test capability that can simultaneously:

- Replicate a flight-like environment across Mach regime of interest
 - Mach, Re, Degrees of Freedom, Free from interference
 - Free-Flight testing in transonic regime is not possible in current ground facilities
- Provide controlled and understood initial conditions
- Provide a detailed history of the vehicle state
 - Forces and moments, vehicle orientation and rotation rates, surface pressure
- Allow for enough test repeats to generate statistically significant set of observations
 - Oscillatory behavior is driven by interaction with the wake, making it inherently stochastic
 - Each shot in a ballistic range produces few oscillations in α_T

Vertical Spin Tunnel (VST)



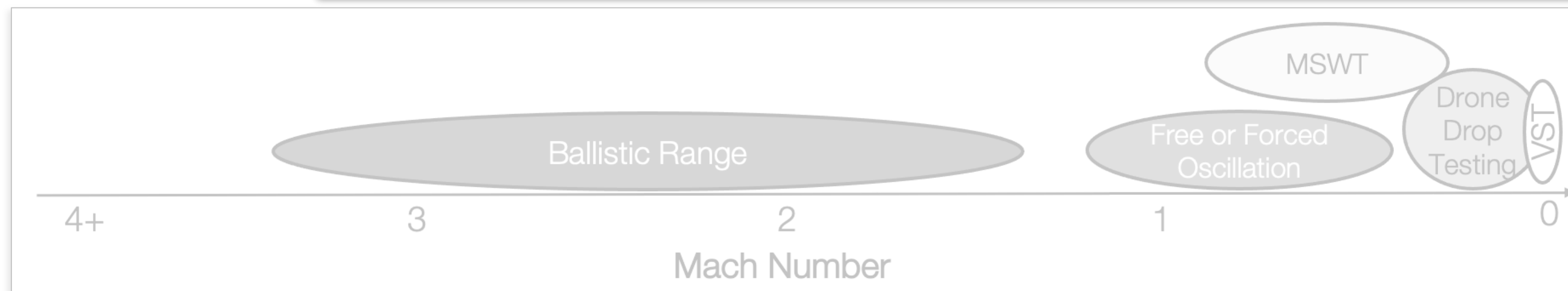
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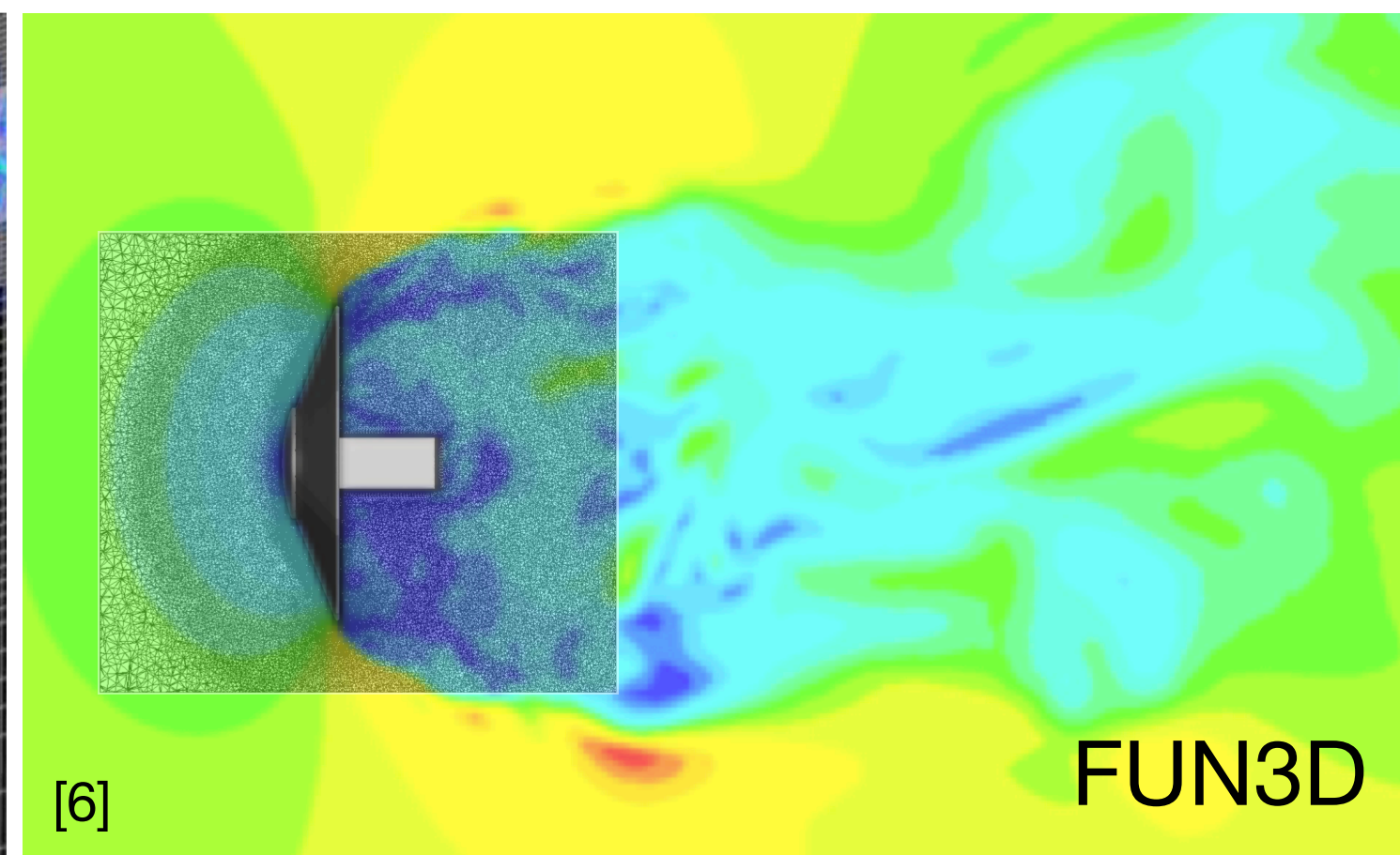
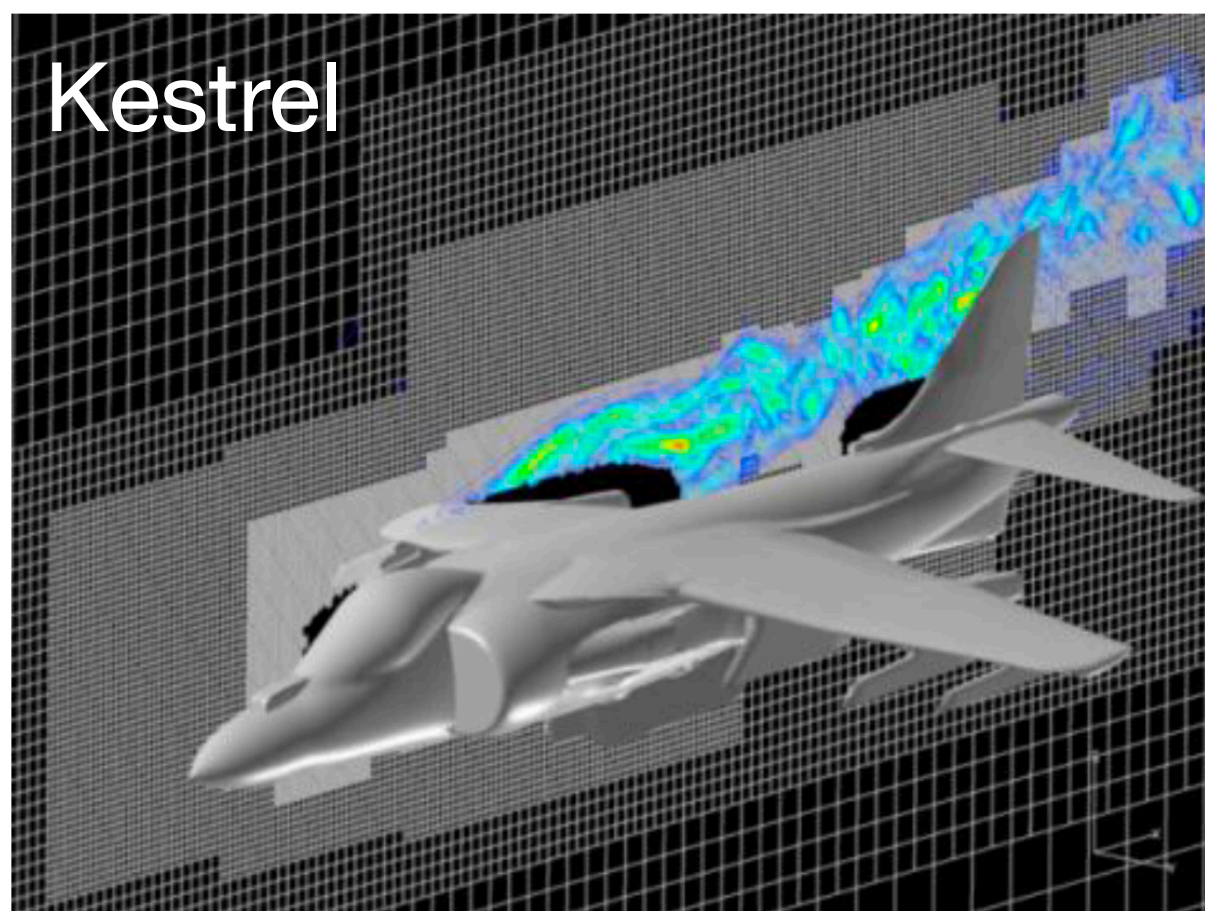
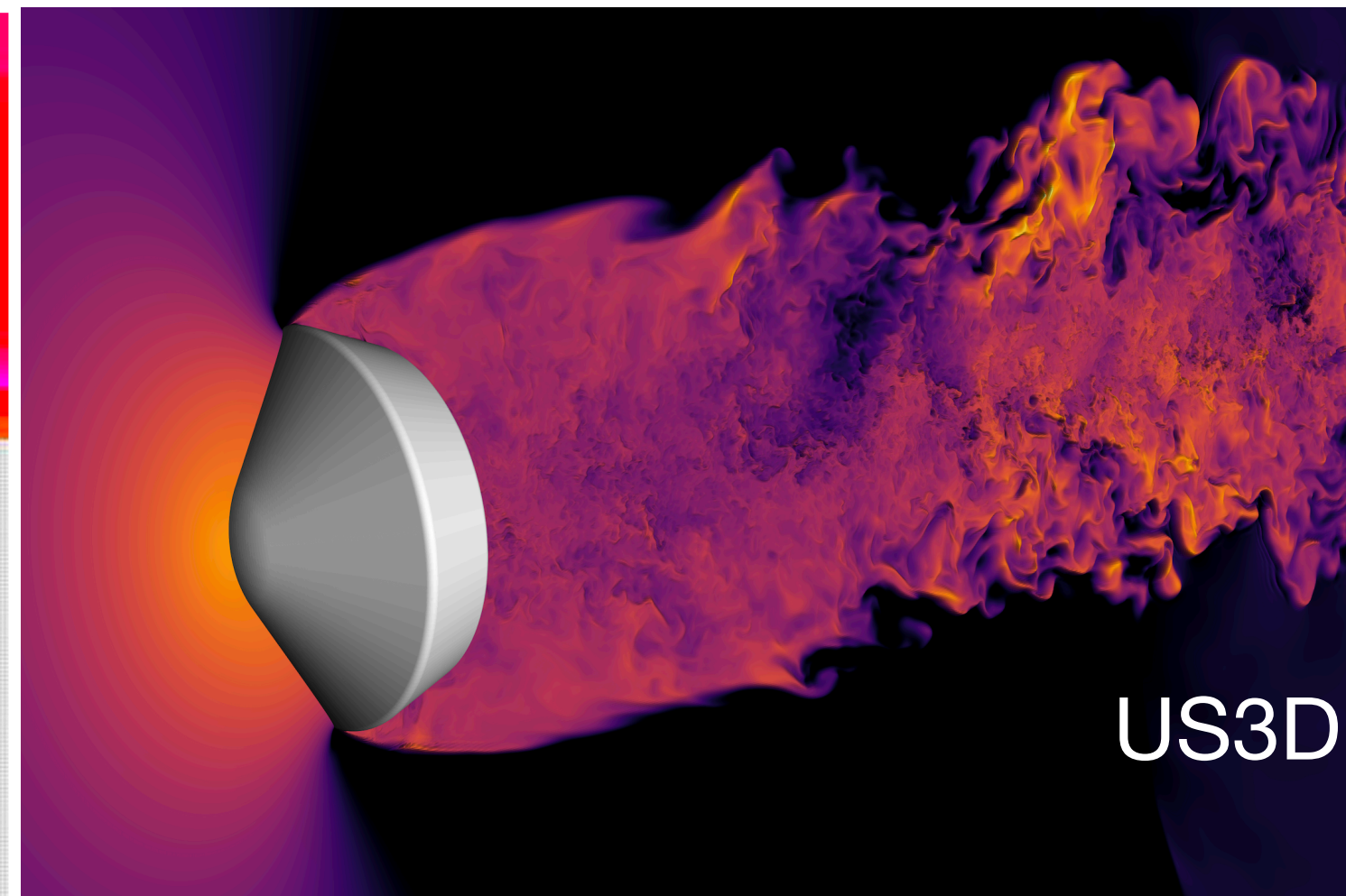
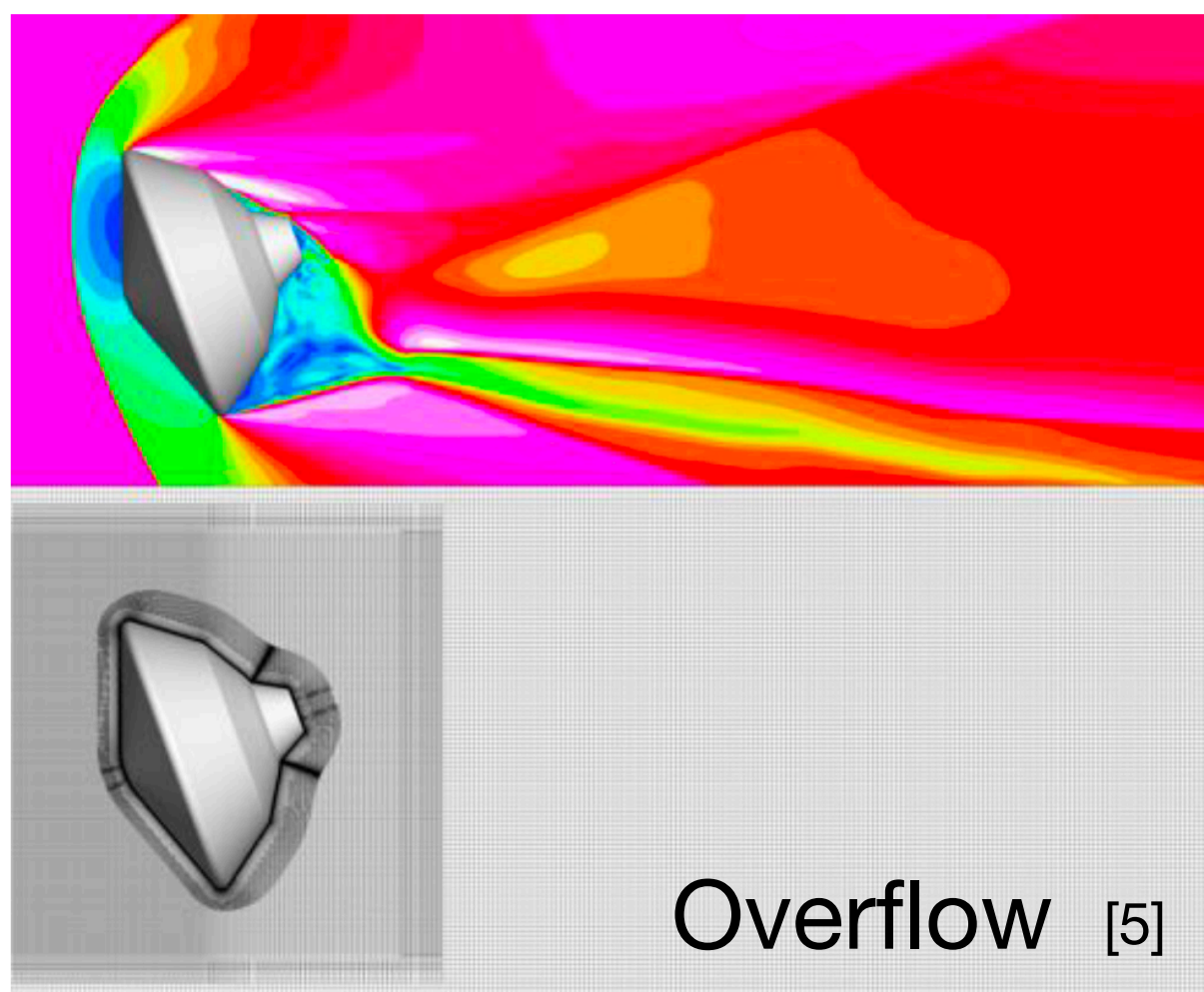
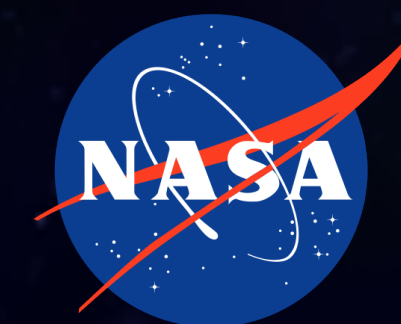
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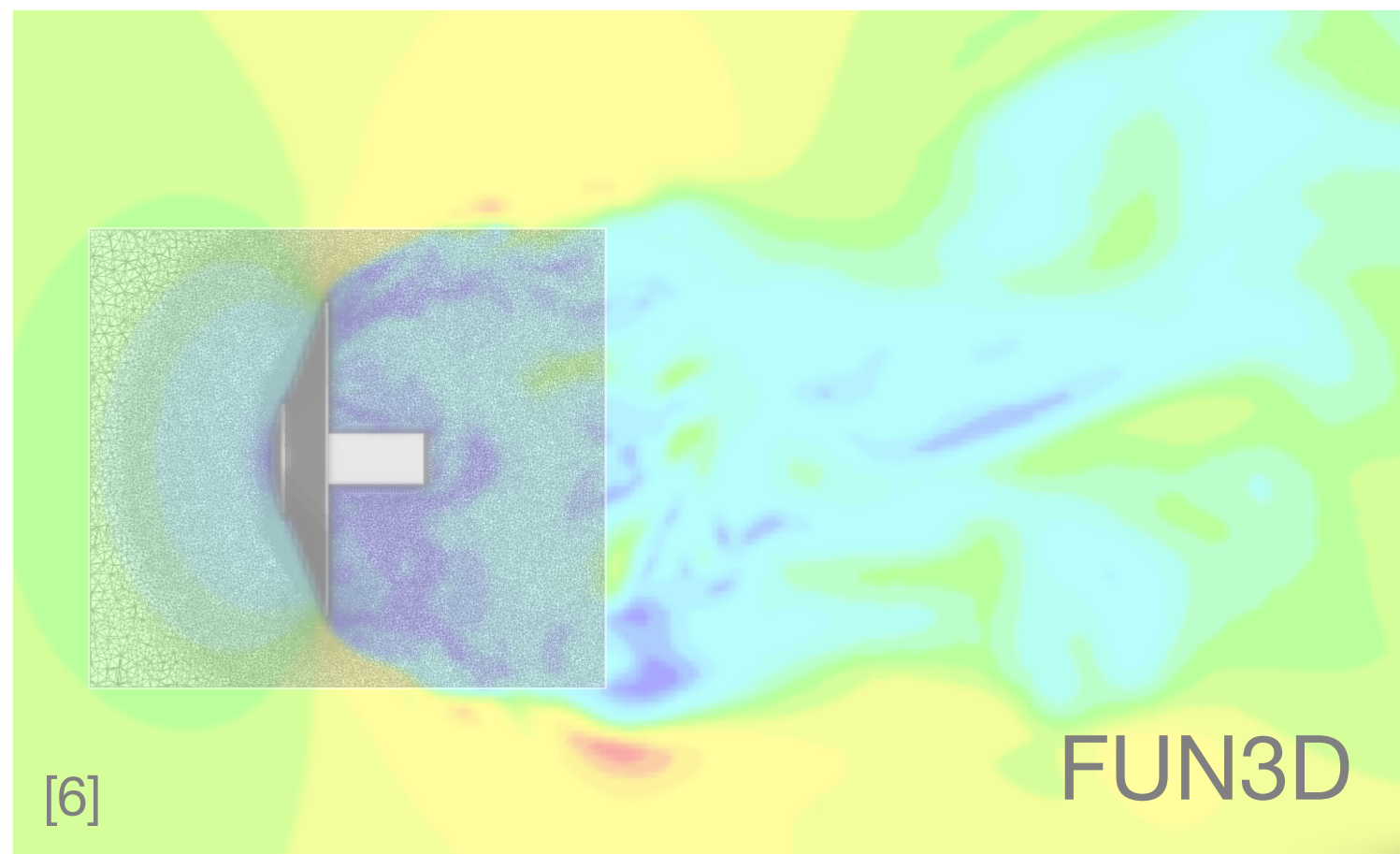
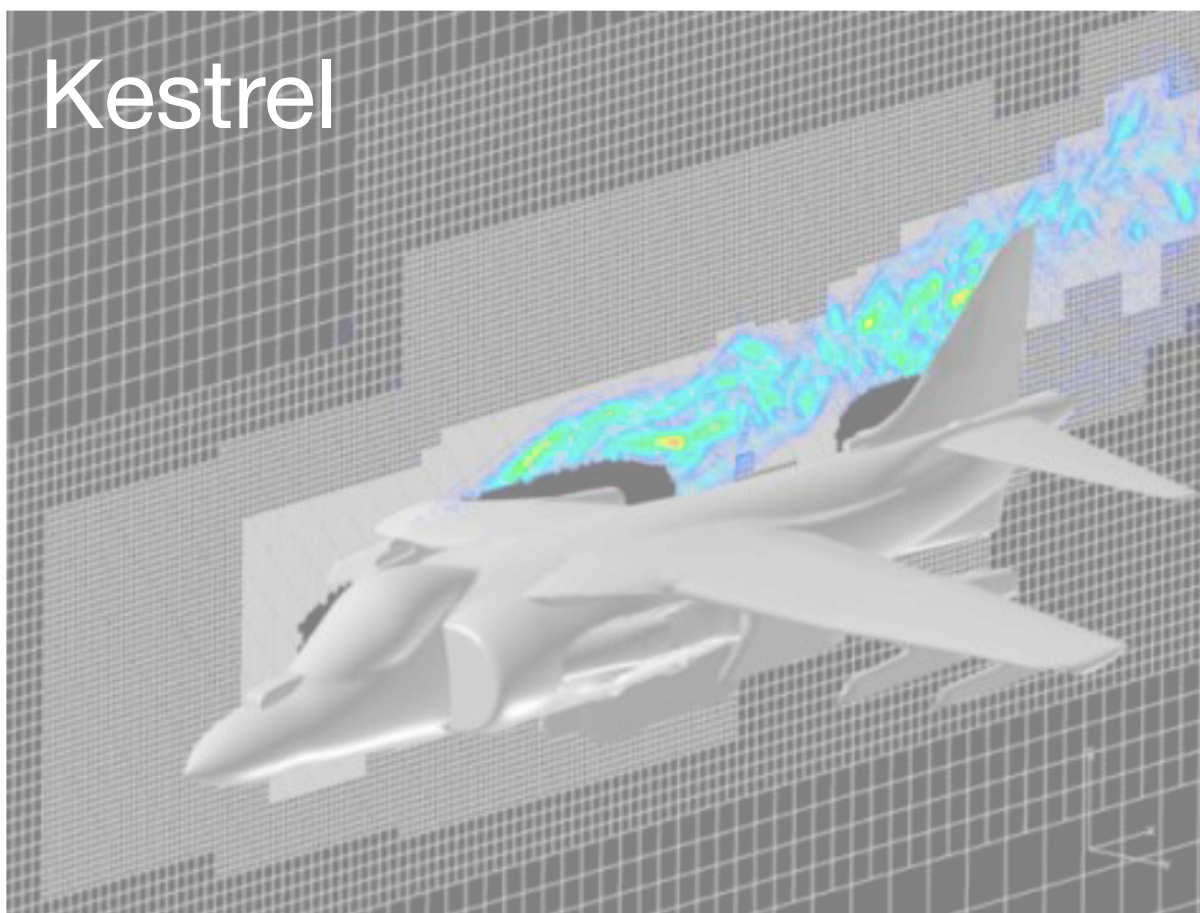
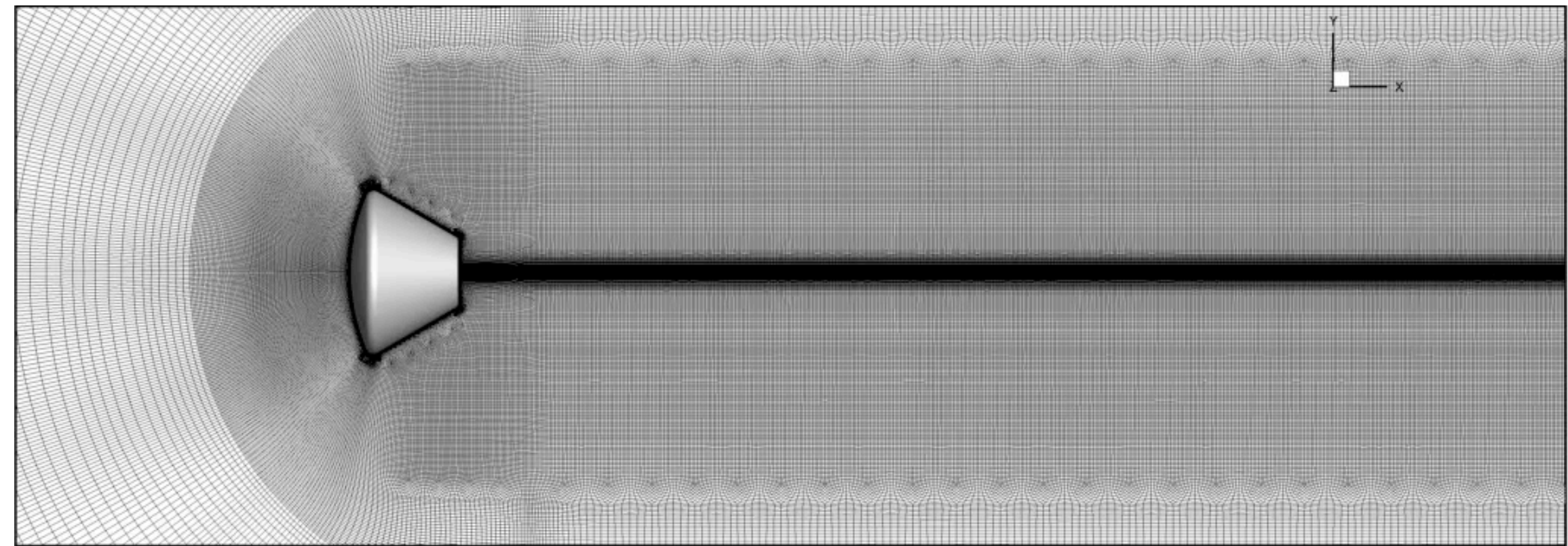
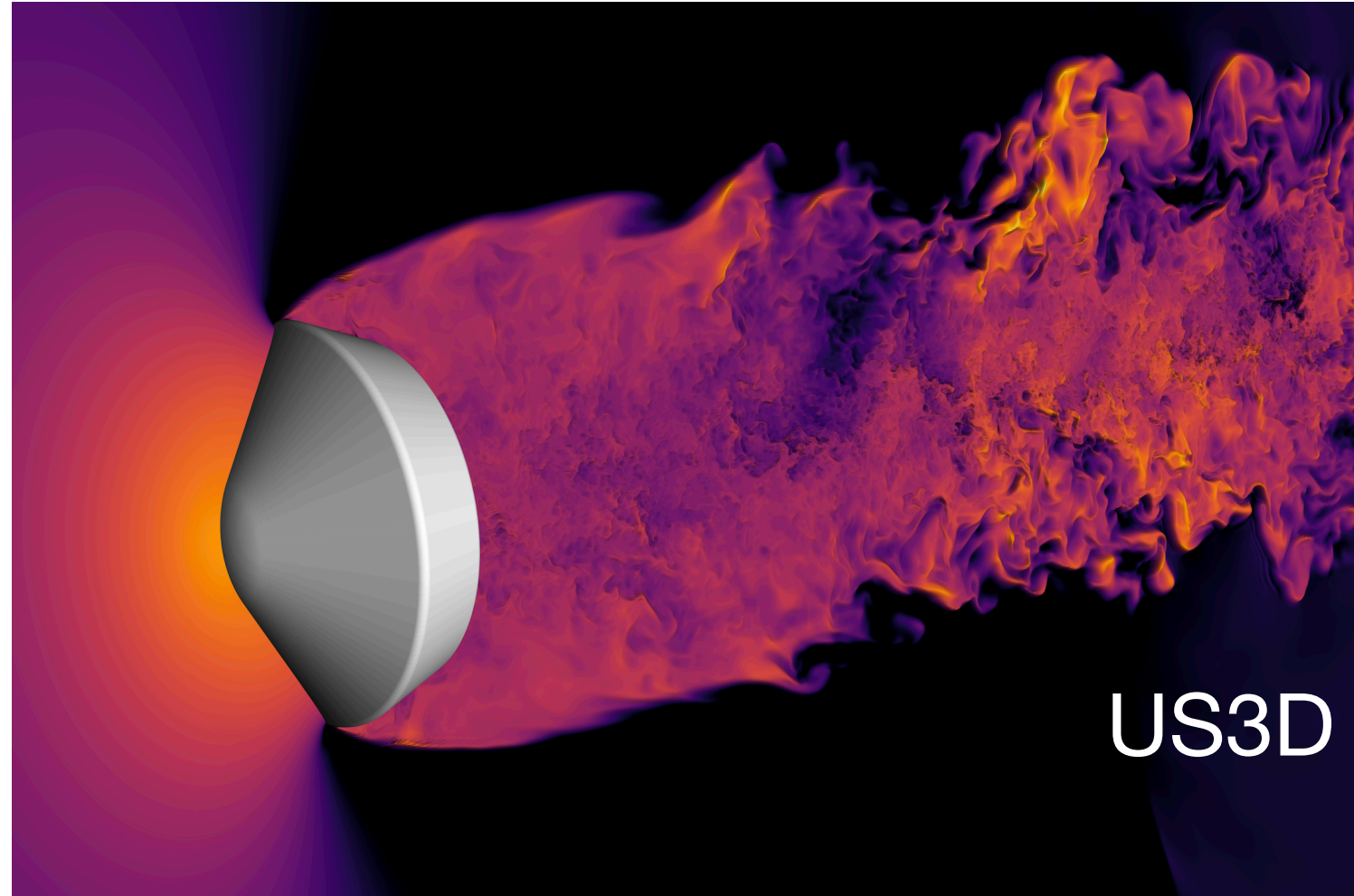
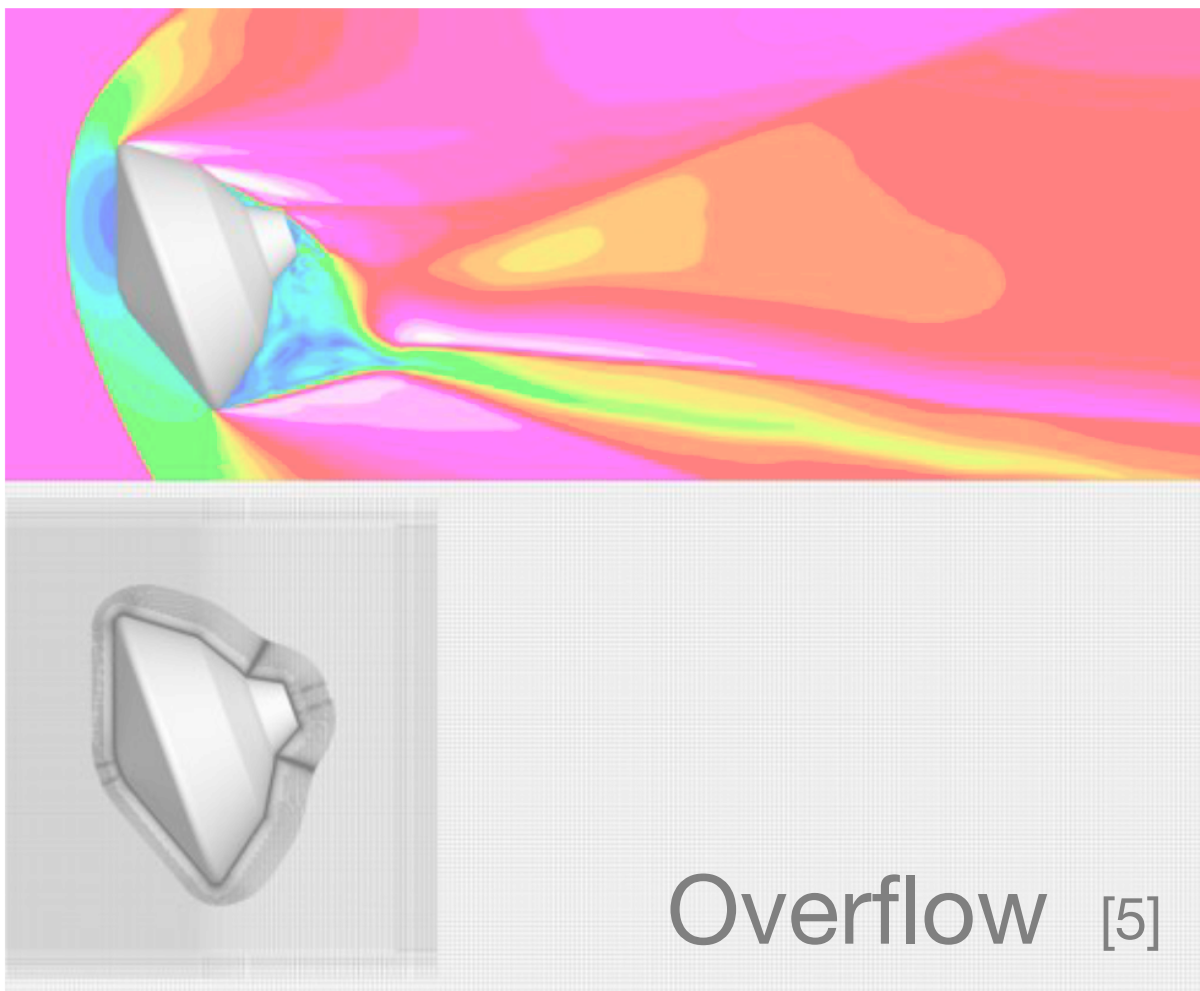
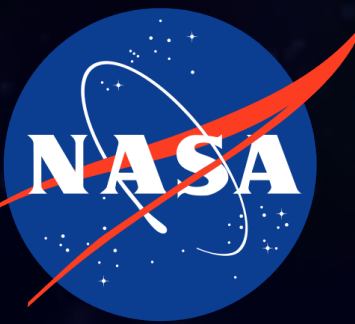


Computational Capabilities



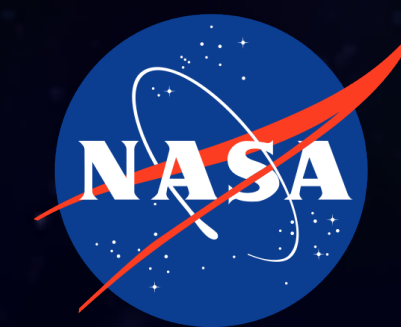
- Inherent constraints in test facilities motivate the development of complementary computational tools
- Several computational codes capable of 6DoF motion are emerging
 - Dynamic motion allows for simulations of forced and free-flying behavior of entry vehicles
- Simulation software verified with experiments will be used to generate dynamic databases anchored with experimental results
- Multiple tool sets provide wide range of Mach numbers and flow regimes to be analyzed

Computational Capabilities

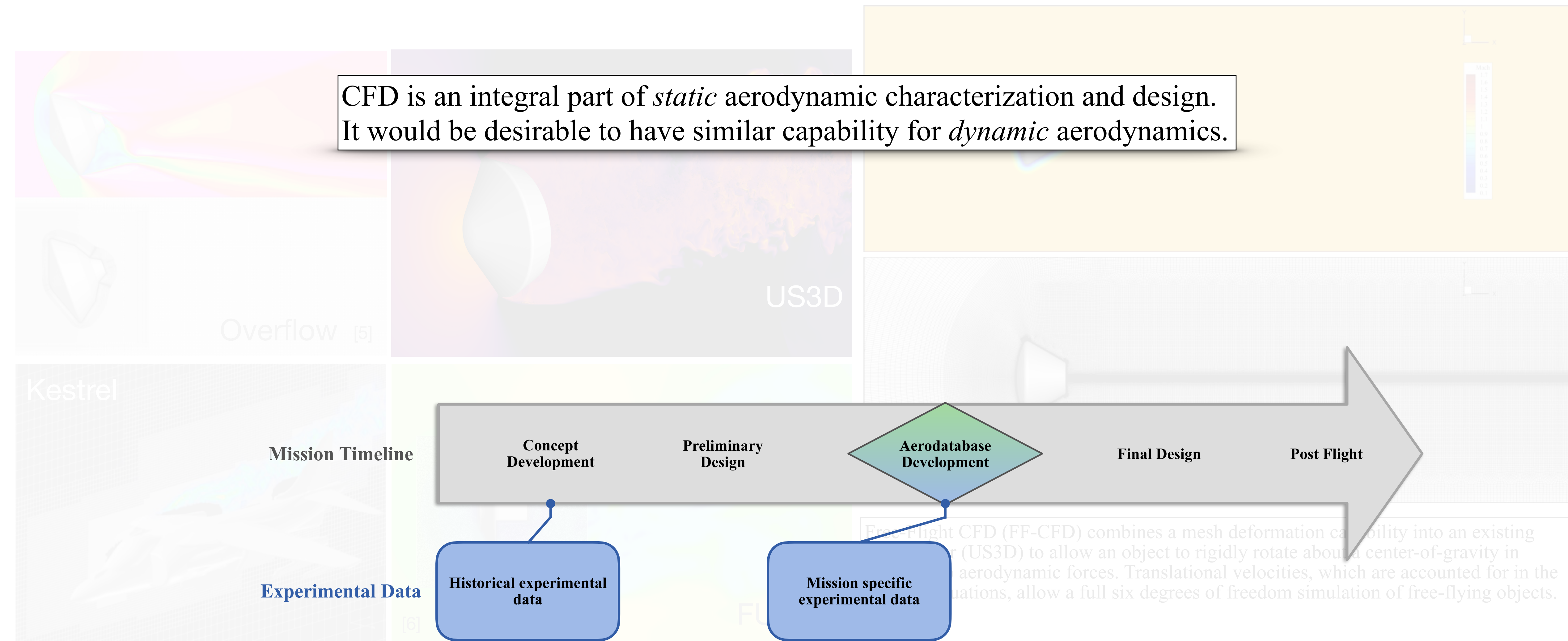


Free-Flight CFD (FF-CFD) combines a mesh deformation capability into an existing CFD solver (US3D) to allow an object to rigidly rotate about a center-of-gravity in response to aerodynamic forces. Translational velocities, which are accounted for in the discrete equations, allow a full six degrees of freedom simulation of free-flying objects.

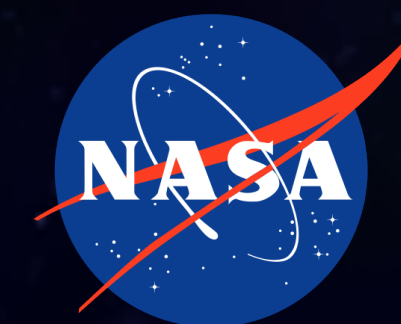
Computational Capabilities



CFD is an integral part of *static* aerodynamic characterization and design. It would be desirable to have similar capability for *dynamic* aerodynamics.



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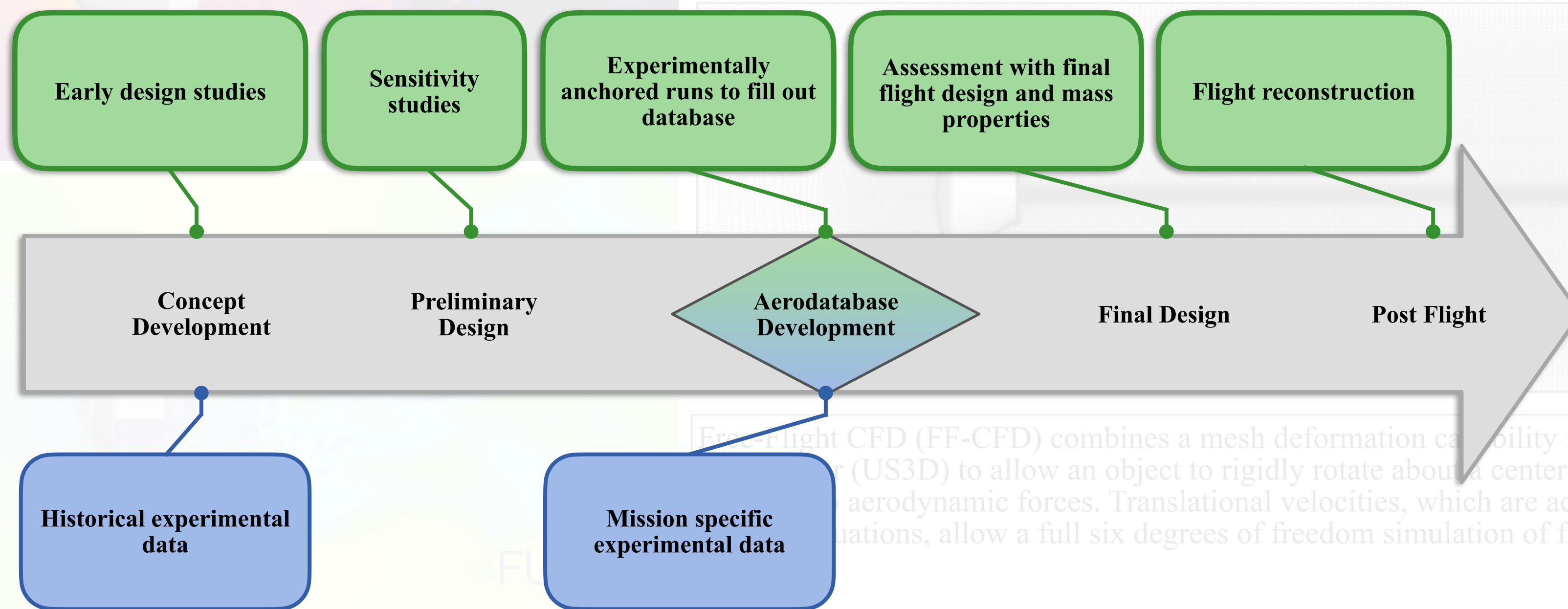
FF-CFD

Overflow [5]

Kestrel

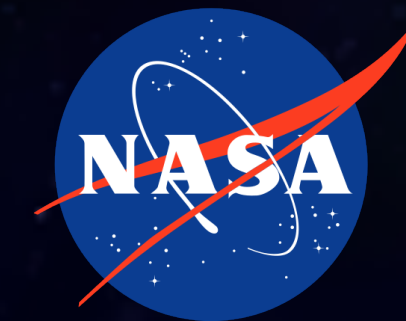
Mission Timeline

Experimental Data

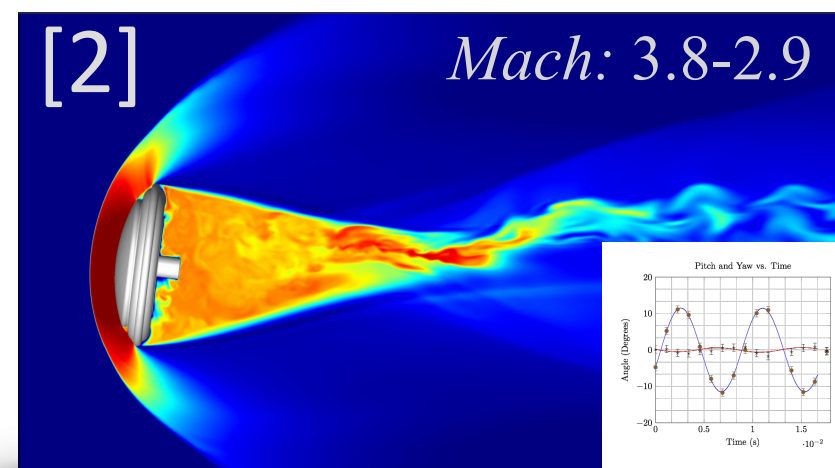
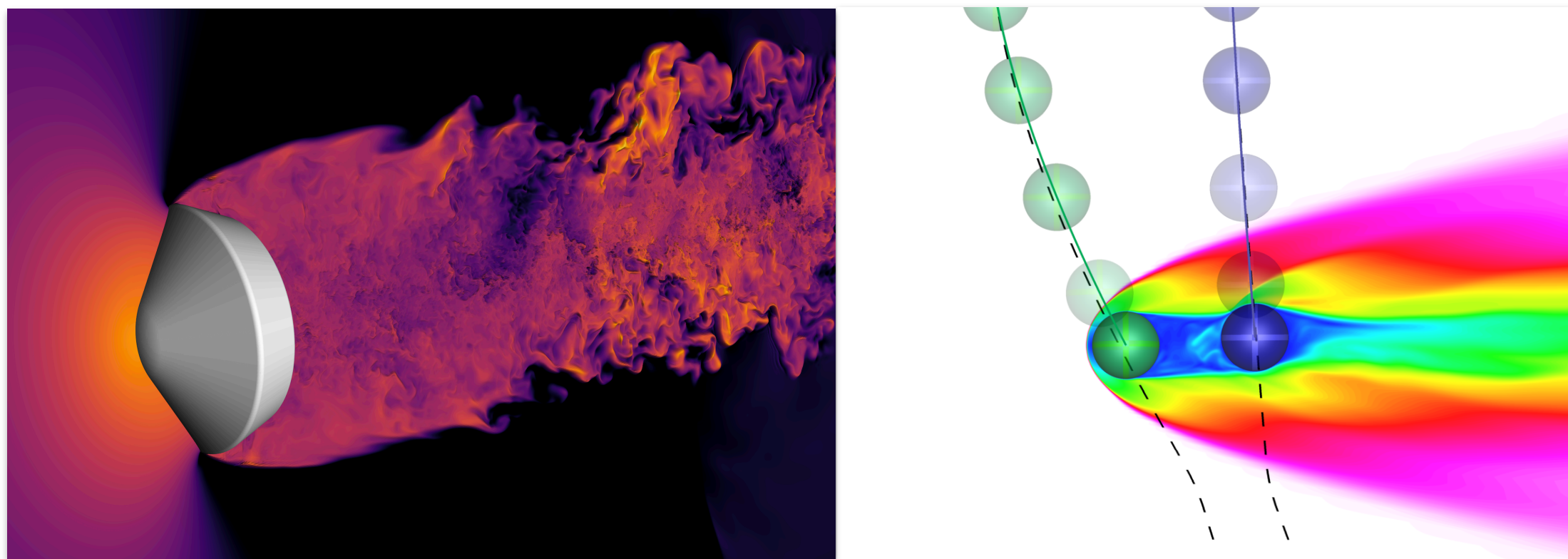


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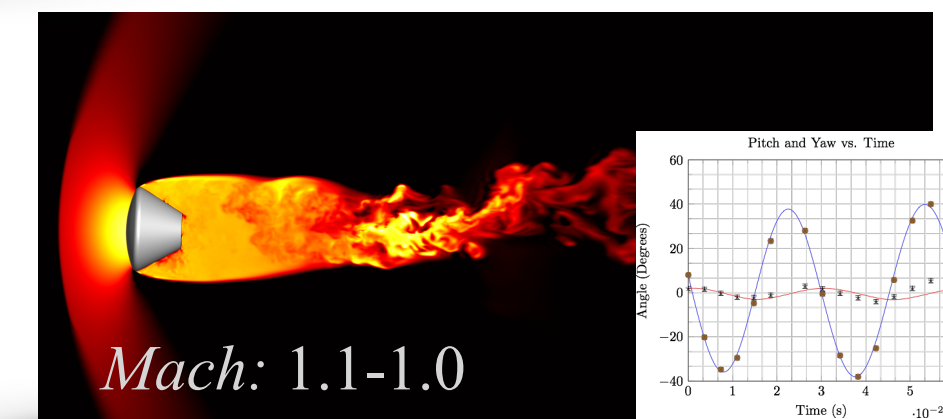
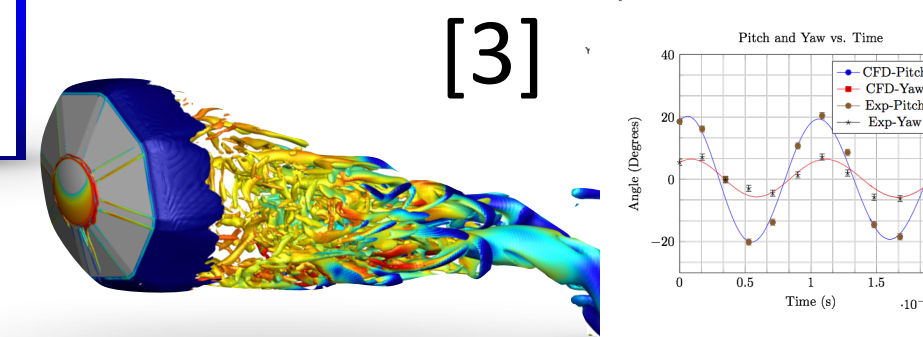
Current State of the Art



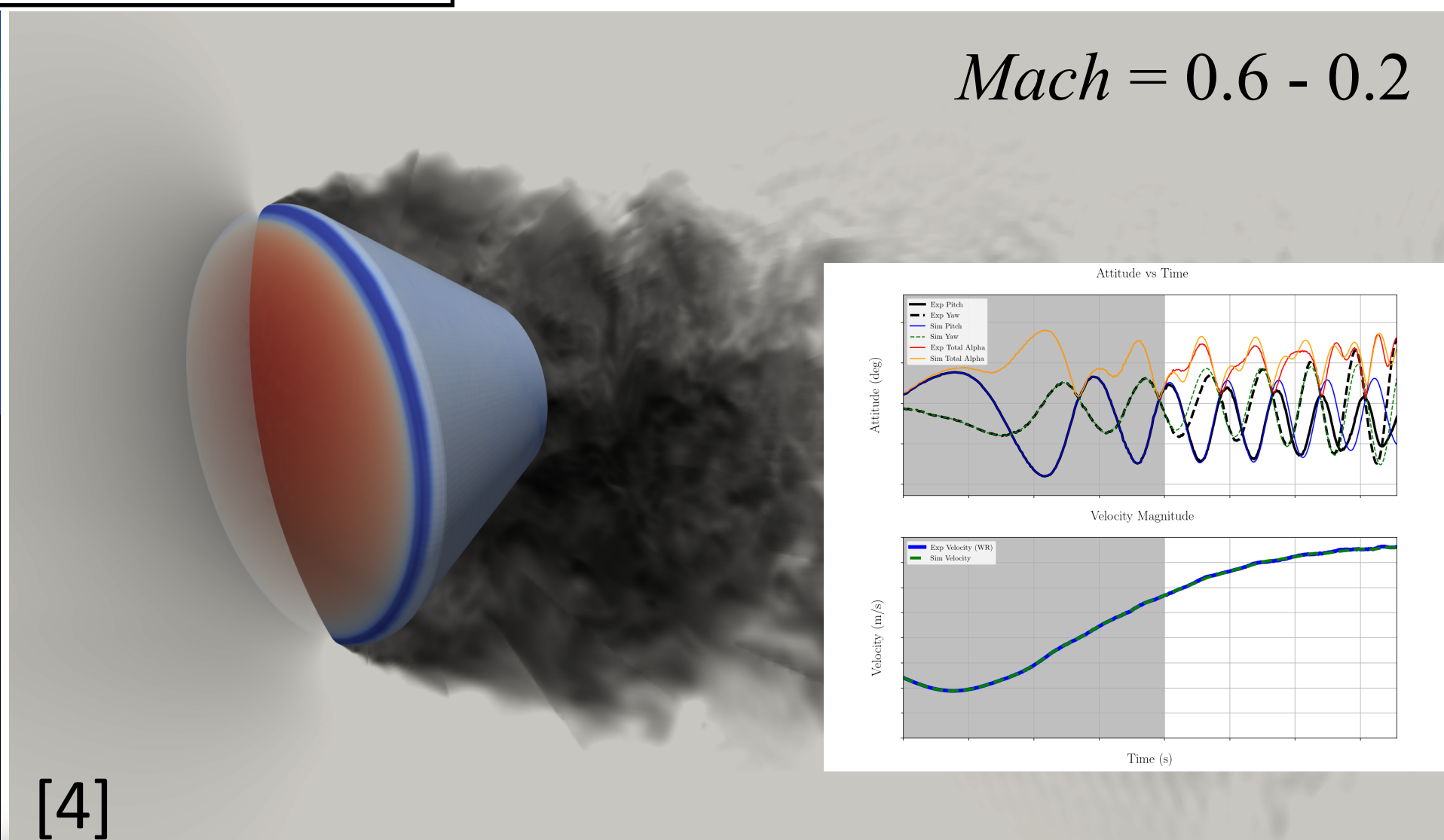
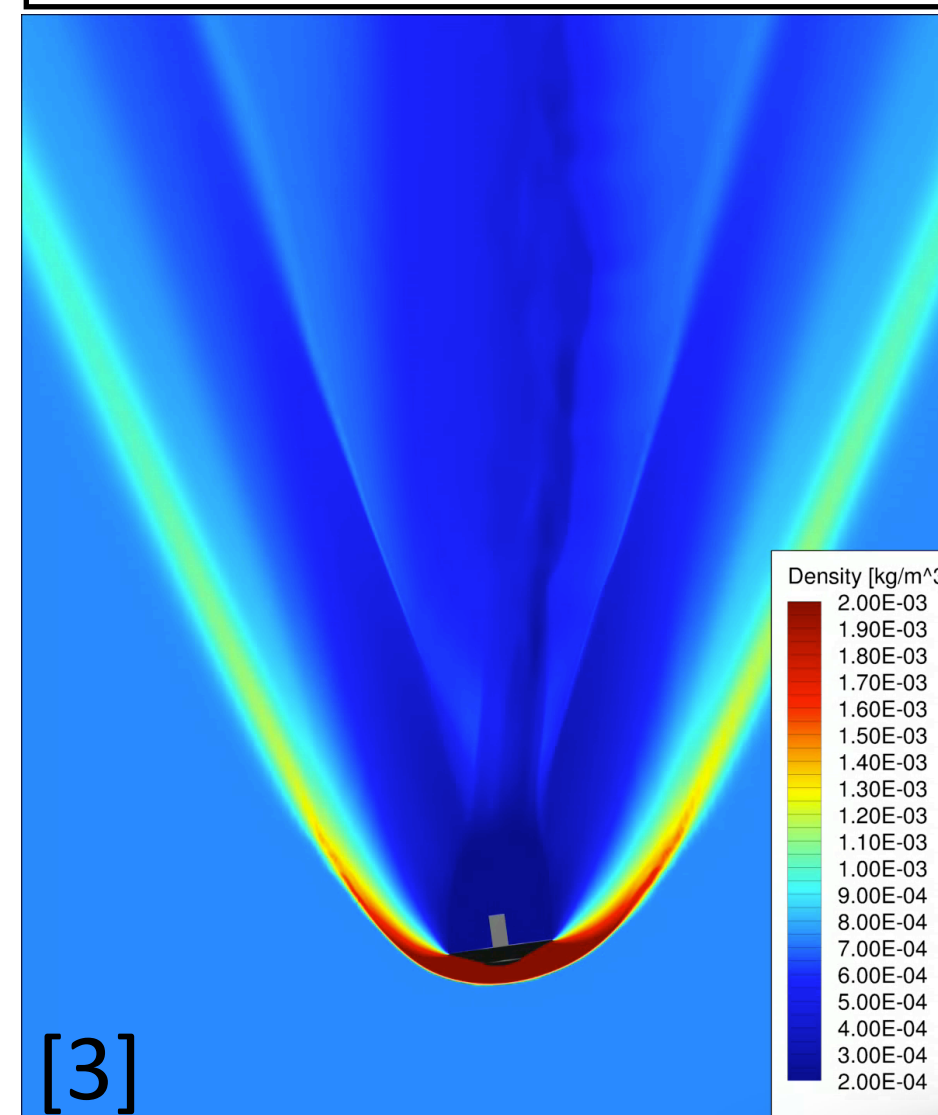
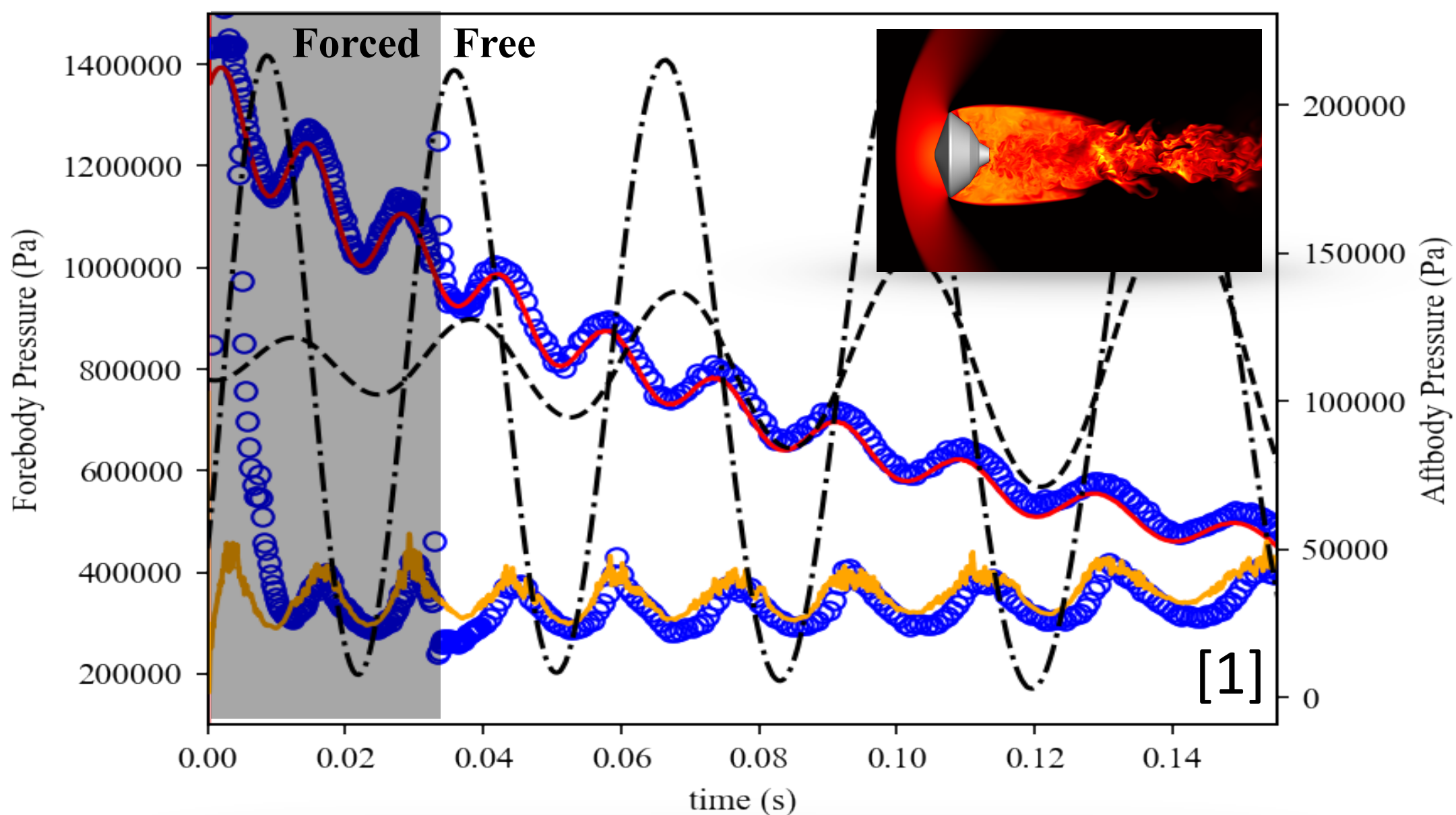
Single/Multi-body Dynamics



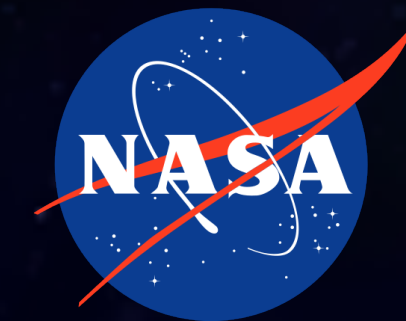
Validated against Experiment



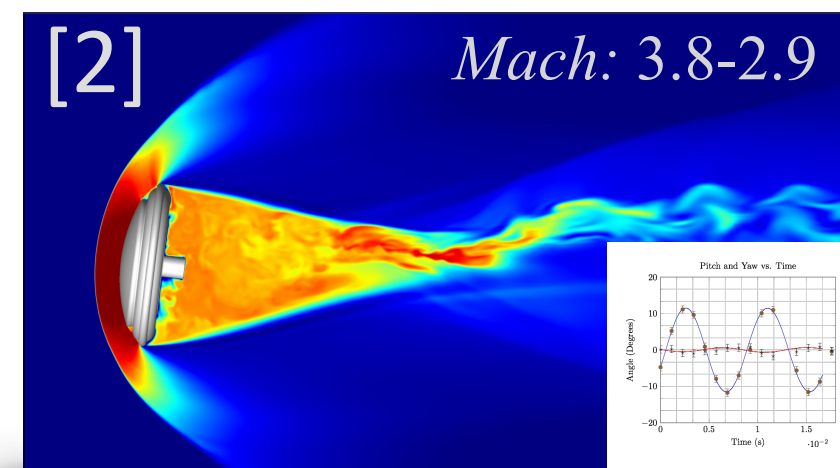
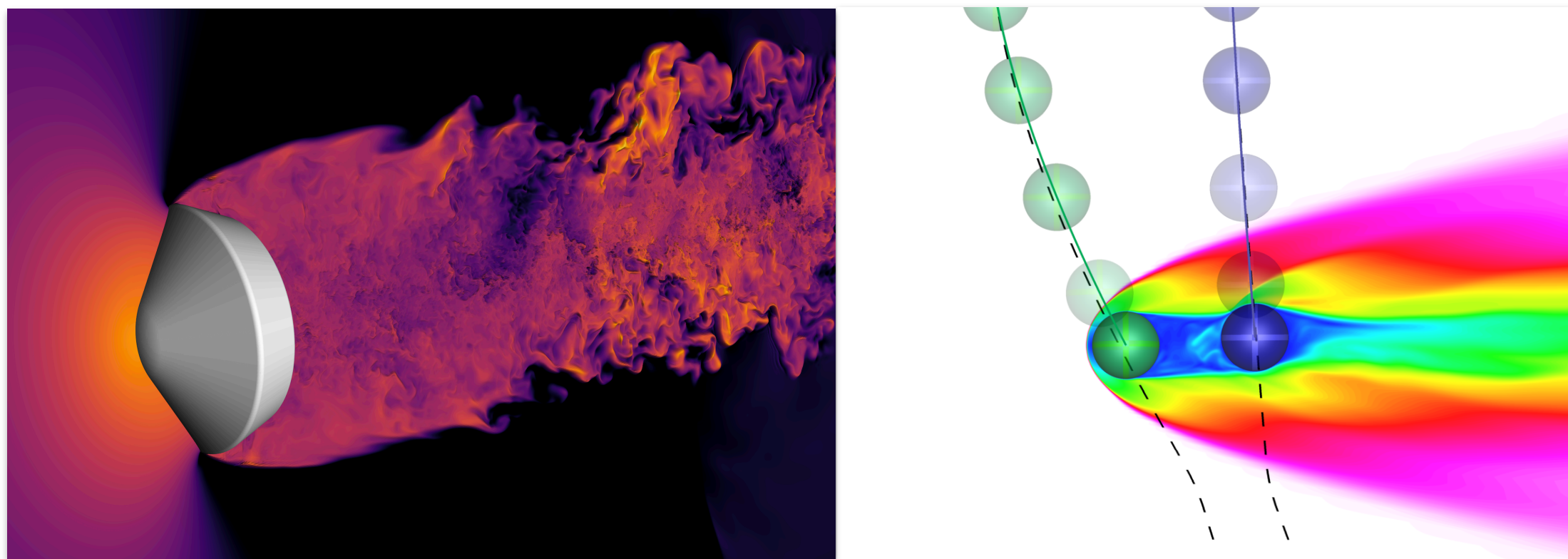
Atmospheric Flight with EarthGRAM



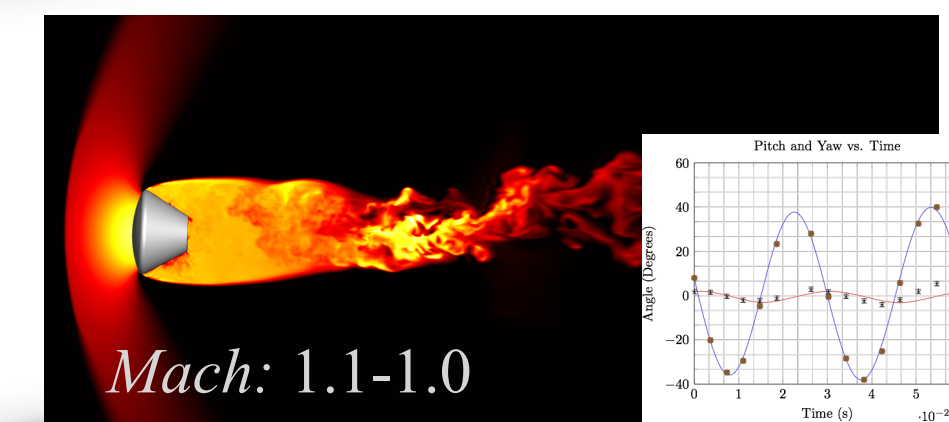
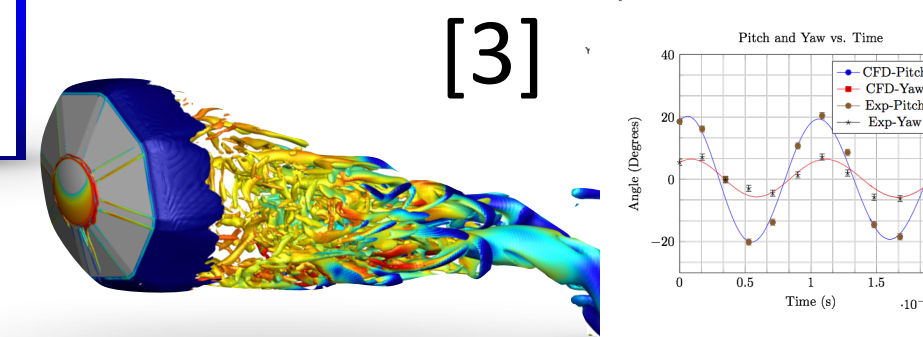
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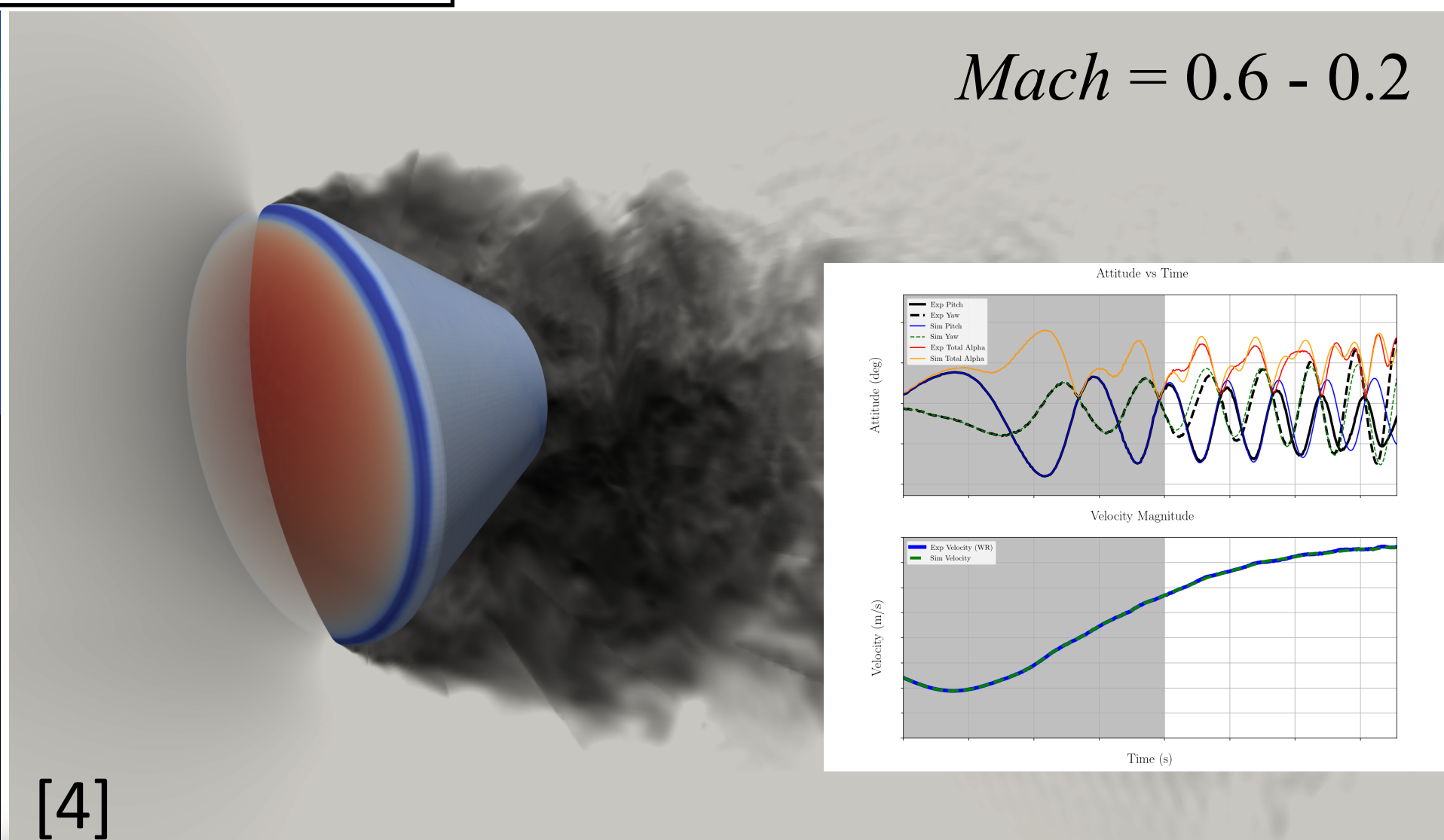
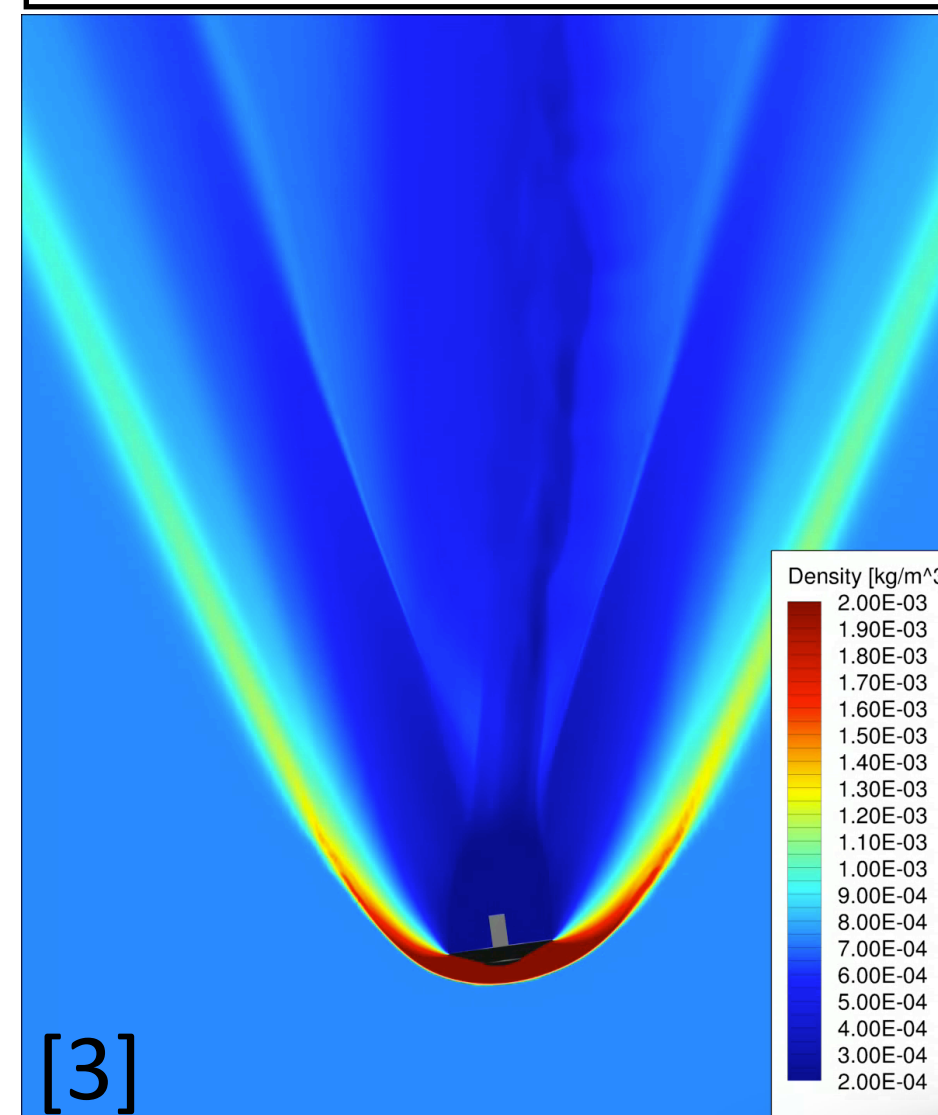
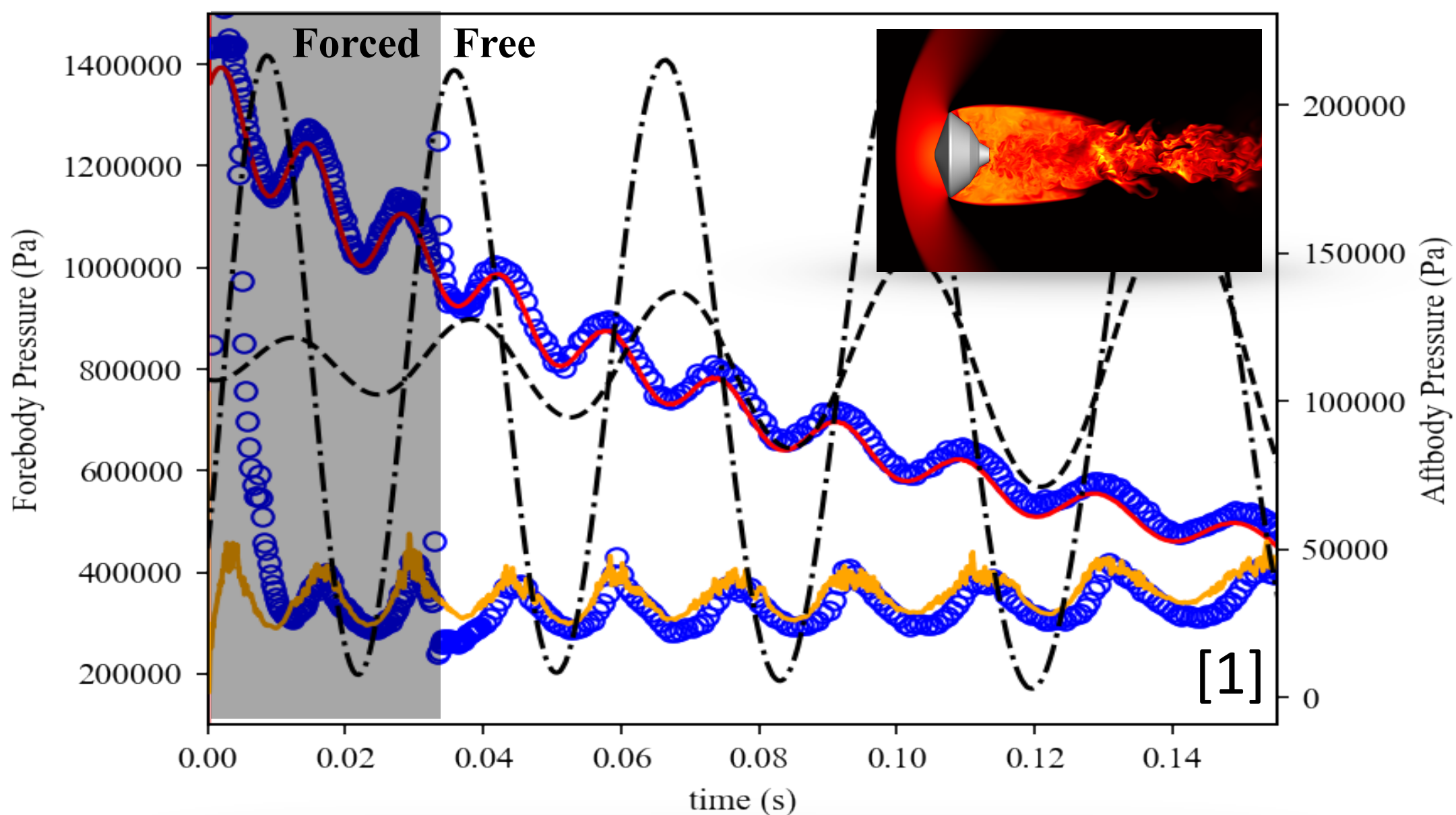
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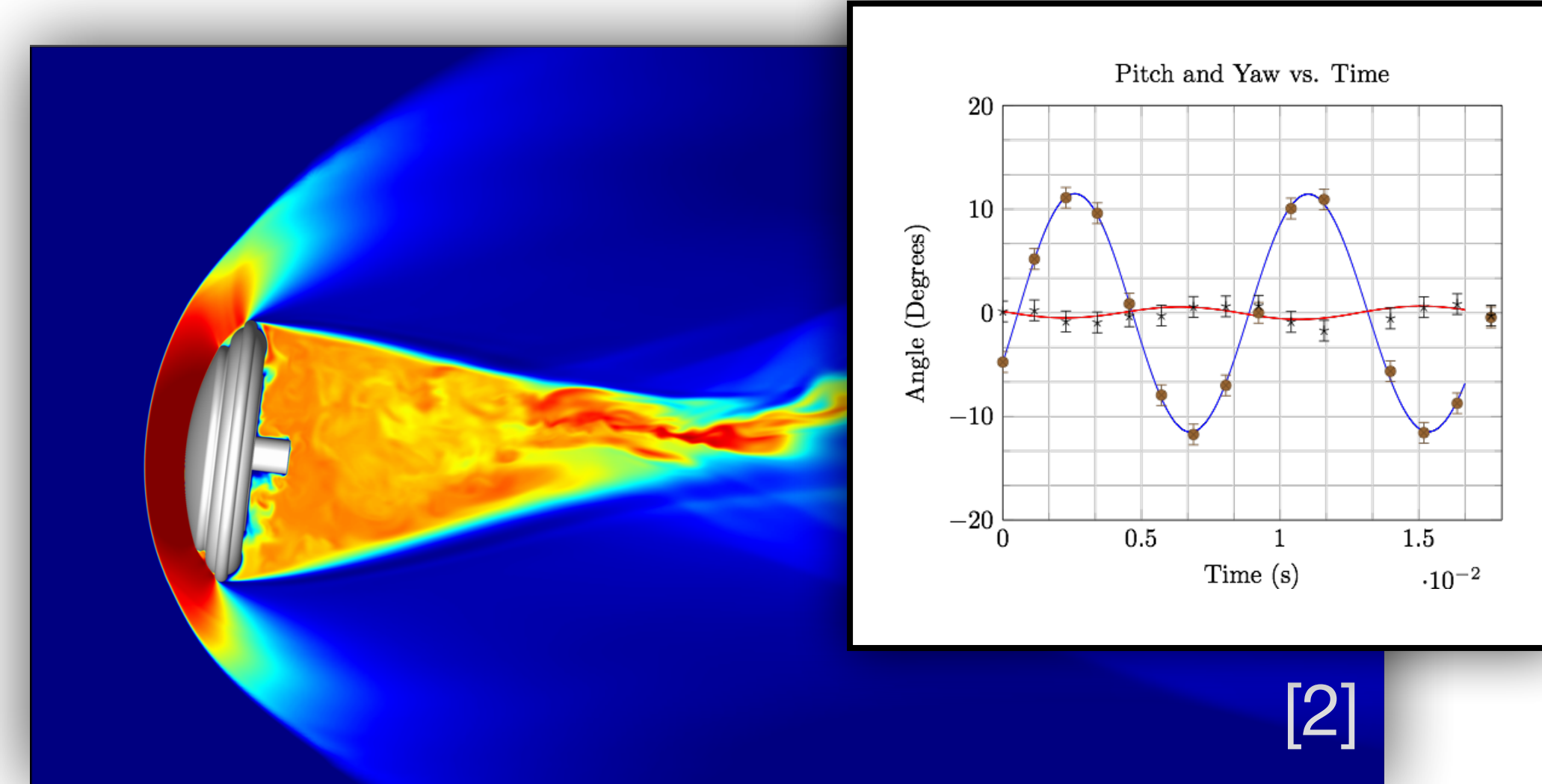
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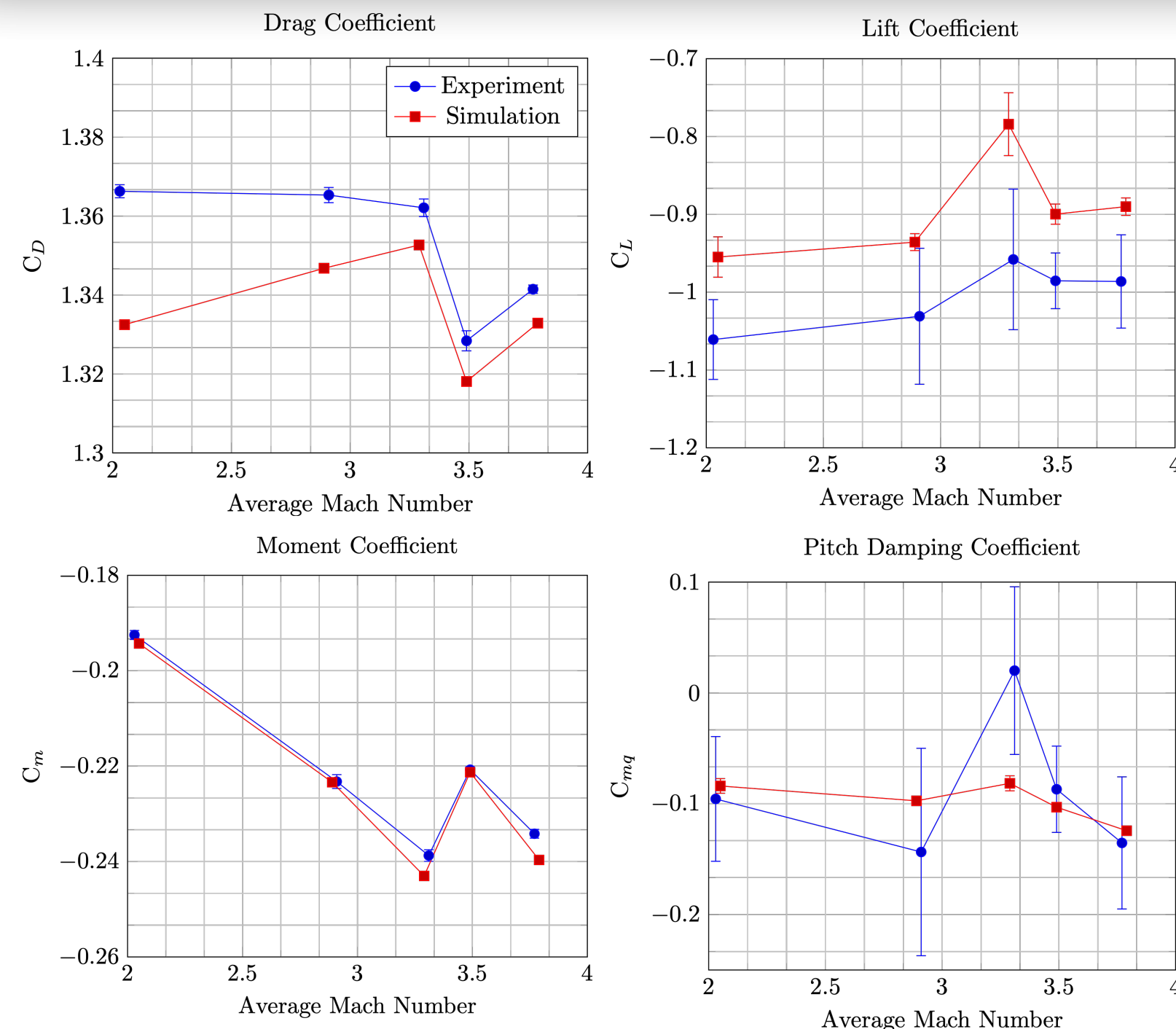
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Free-Flight CFD Data as Input to Heritage Methods

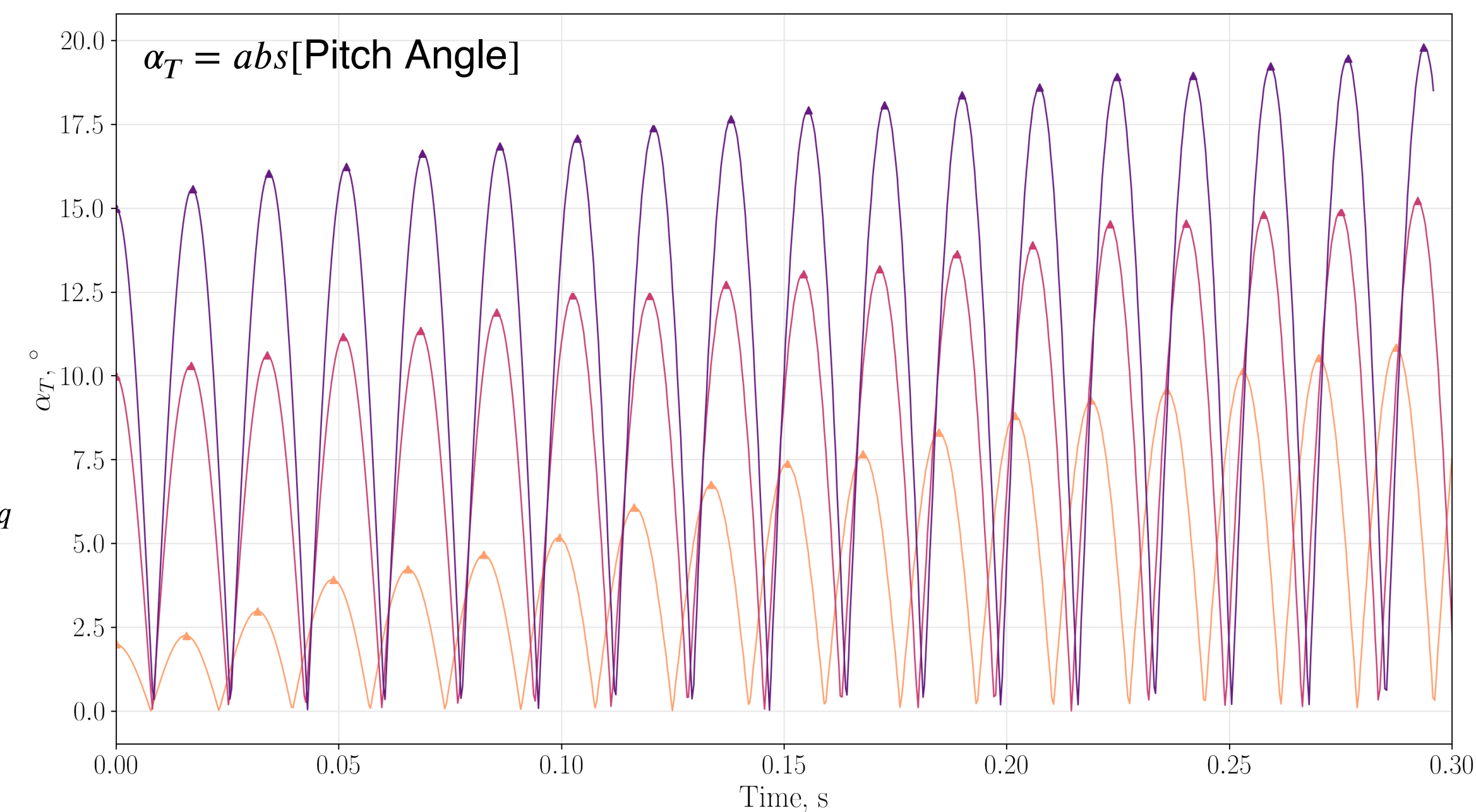
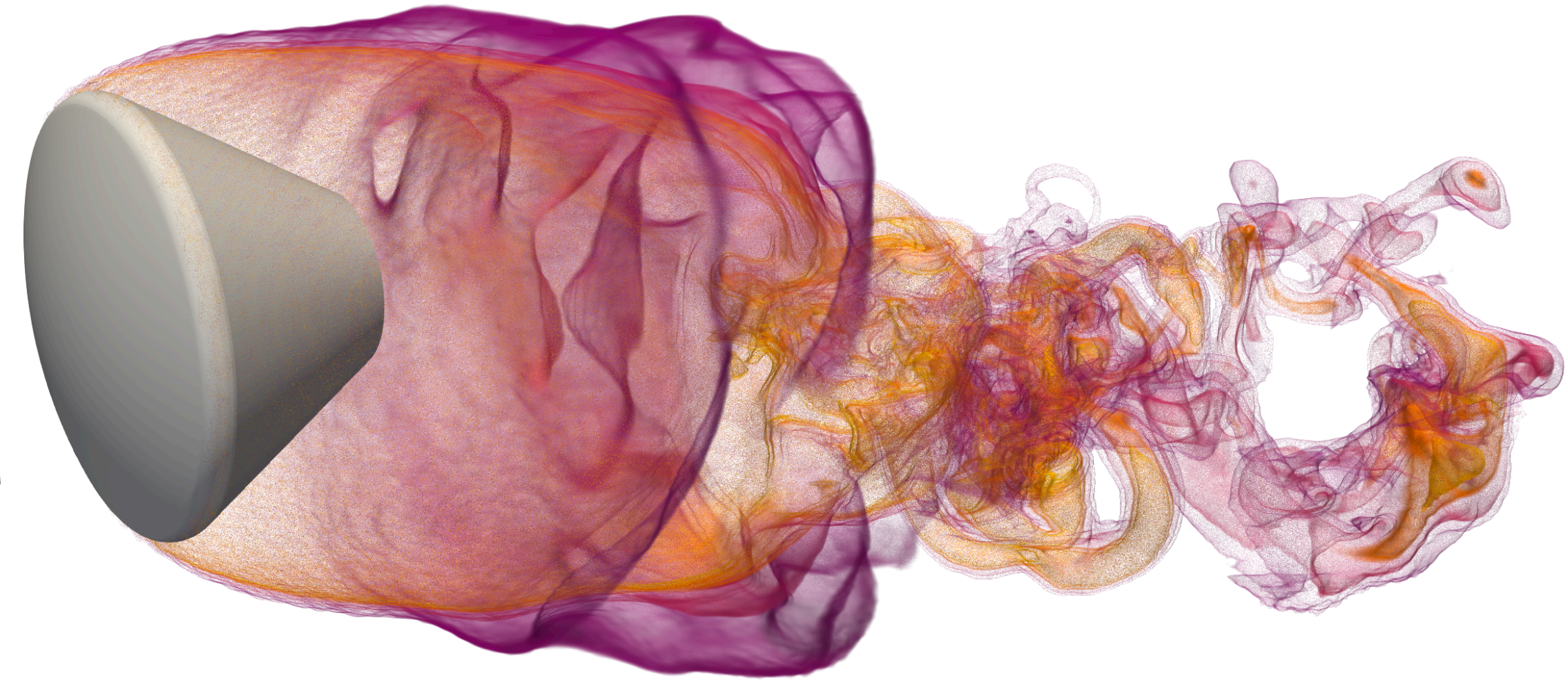


- Dynamic stability is often characterized by the pitch damping coefficient (C_{m_q})
- Derivations of pitch damping coefficient in previous studies were obtained using the aerodynamic software CADRA
 - Results shows good comparison between simulation and ballistic range results
 - Required significant coarsening from order 100,000 time steps of CFD data down to 16 data points to obtain 1-to-1 comparison with BR data
- Rich datasets from FF-CFD simulations present an opportunity to apply new data reduction approaches



Data Reduction for Free-Flight CFD

- **PYnamics** software suite to process FF-CFD output
 - A python suite of tools available to post-process FFCFD data and generate static and dynamic aero-coefficients
- Schoenenberger [5] states that (within assumptions of derived models) an equivalent C_{m_q} can be derived from 1- 2- or 3-DoF simulations
- Two methods developed for using FF-CFD 1-DoF analysis to computing dynamic coefficients
 1. Run reduced 1DoF FF-CFD simulations and then:
 - 2a. Use analytical forms of equations to generate non-linear fits to C_{m_q} as a function of oscillation amplitude
 - 2b. Use inverse estimation and 1-DoF EOMs to identify optimal C_{m_q} curve as a function of instantaneous angle of attack.

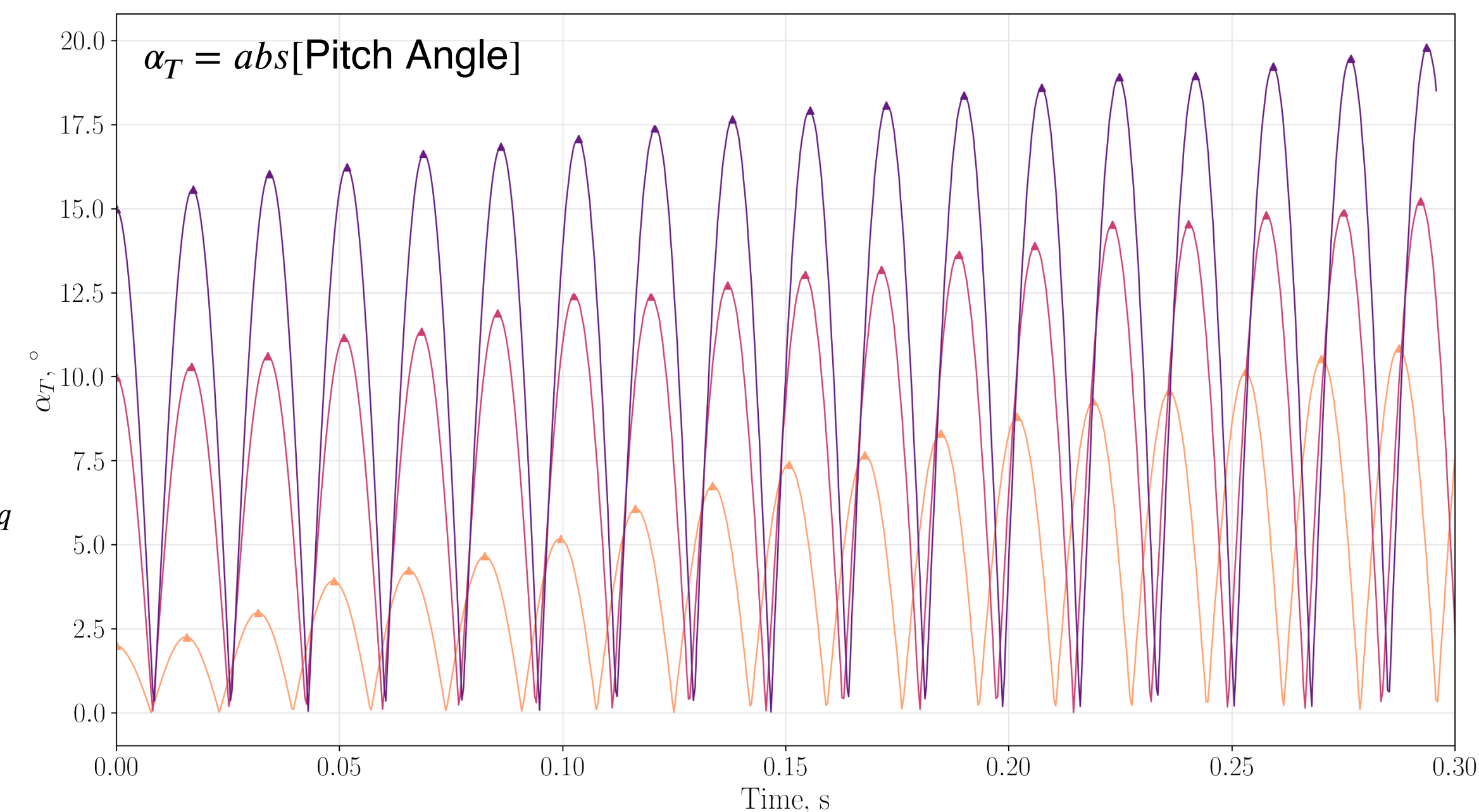
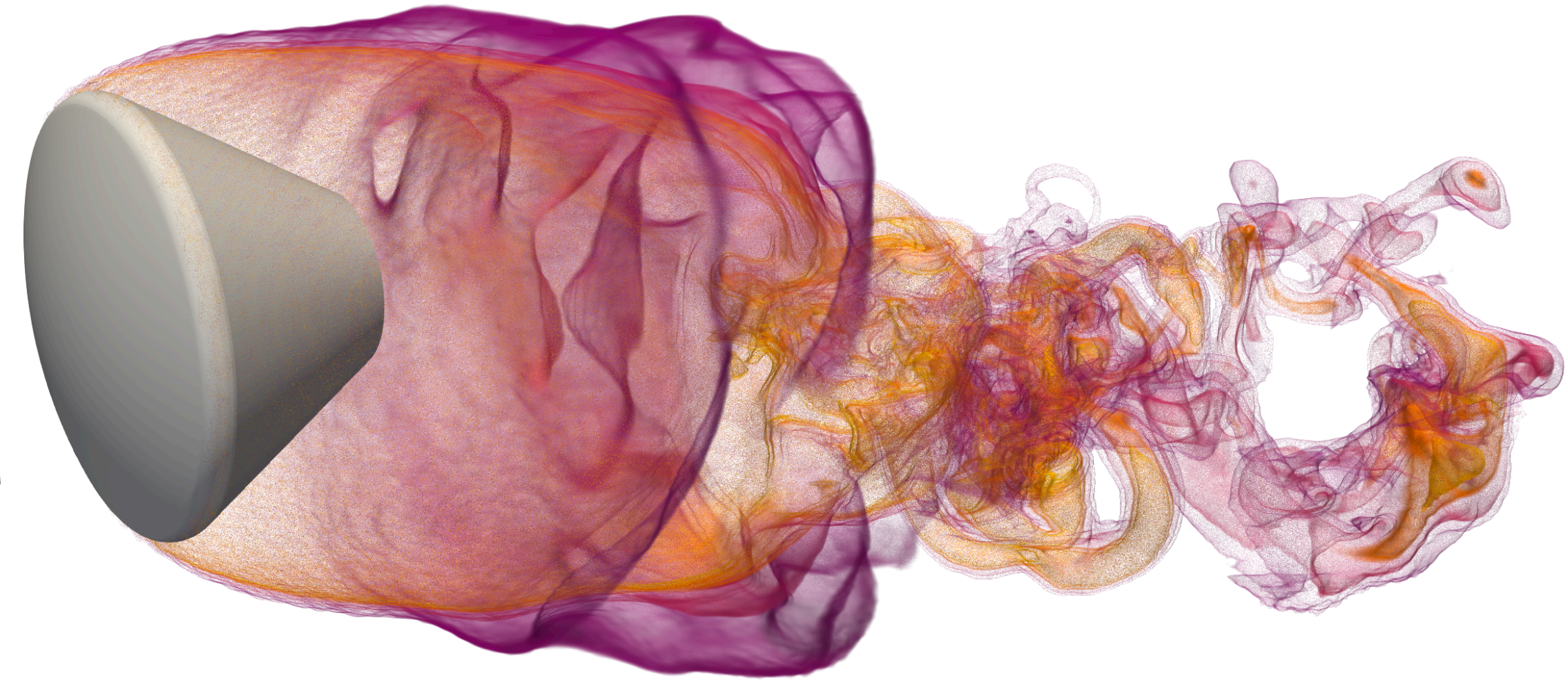


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Use of Analytical Solutions To Compute Pitch Damping

- Methodology for using FF-CFD 1-DoF analysis to compute dynamic coefficients [6]

1-DoF Analytical Solution

$$\ddot{\alpha} - \frac{\rho V_{\infty} S d^2}{4I} (C_{m_q} + C_{m_{\dot{\alpha}}}) \dot{\alpha} - \frac{\rho V_{\infty}^2 S d}{2I} C_{m_{\alpha}} \alpha = 0$$

$$\alpha = A e^{\xi_1 t} \cos(\omega t + \delta) \quad \longrightarrow \quad \xi_1 = \frac{\rho V S d^2}{8I} (C_{m_q} + C_{m_{\dot{\alpha}}})$$

Algorithm:

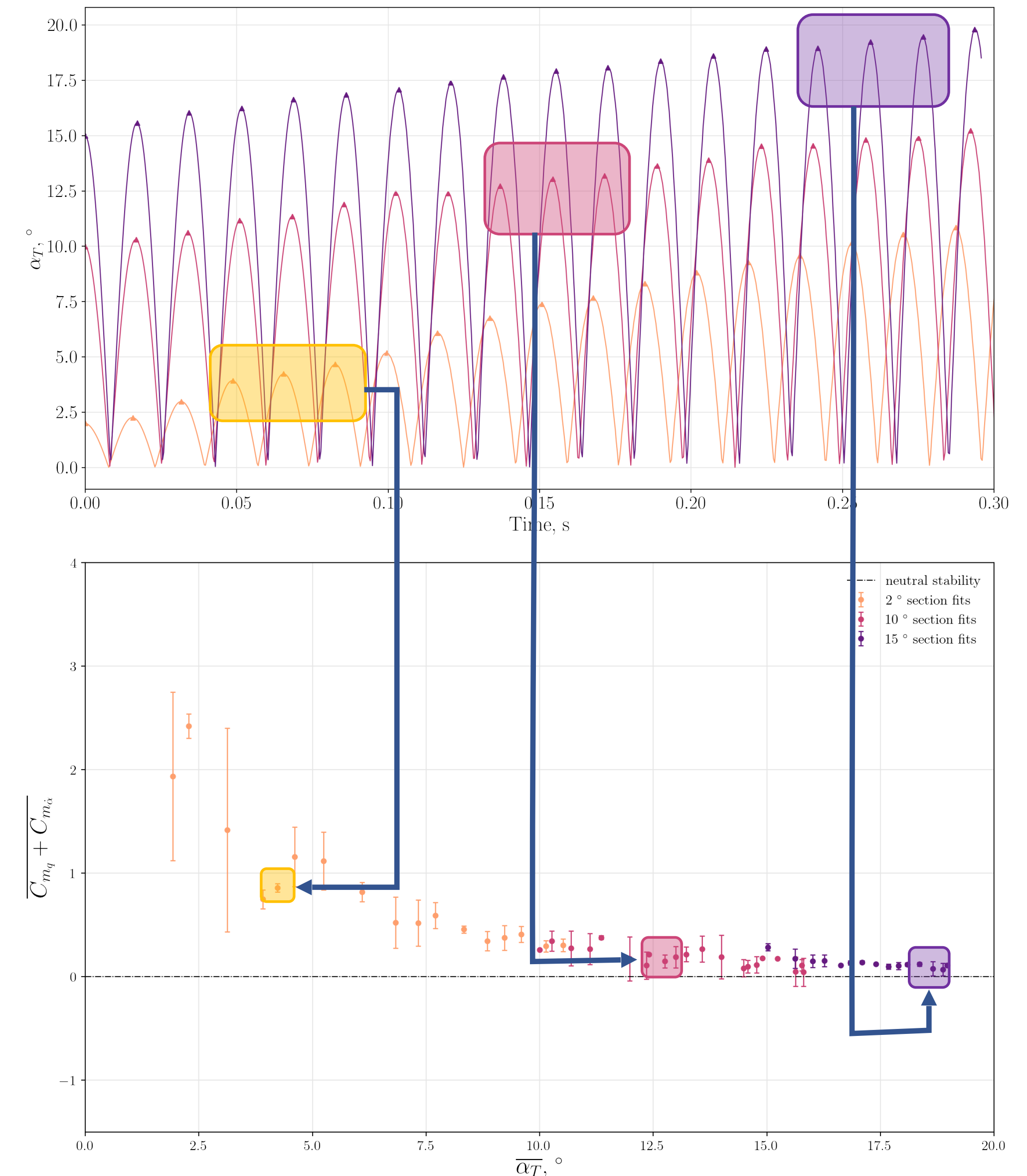
➤ For each α_0 :

- Using a stencil of 3-5 peaks, fit analytical expression for \bar{C}_{m_q} to segments of the trajectory to capture local amplitude growth (or decay)
- Add this \bar{C}_{m_q} value to our larger \bar{C}_{m_q} vs a space at the average total angle of attack for the peaks within that stencil
- Move to next set of stenciled peaks and repeat

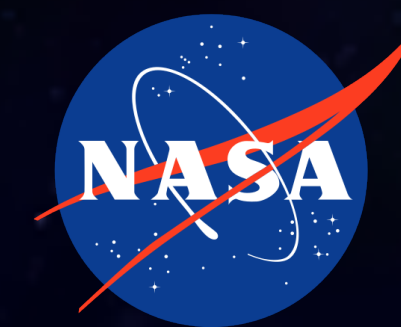
➤ Combine all individual stencil fits into amplitude bins

➤ Curve fit bins to get \bar{C}_{m_q} as a function of amplitude

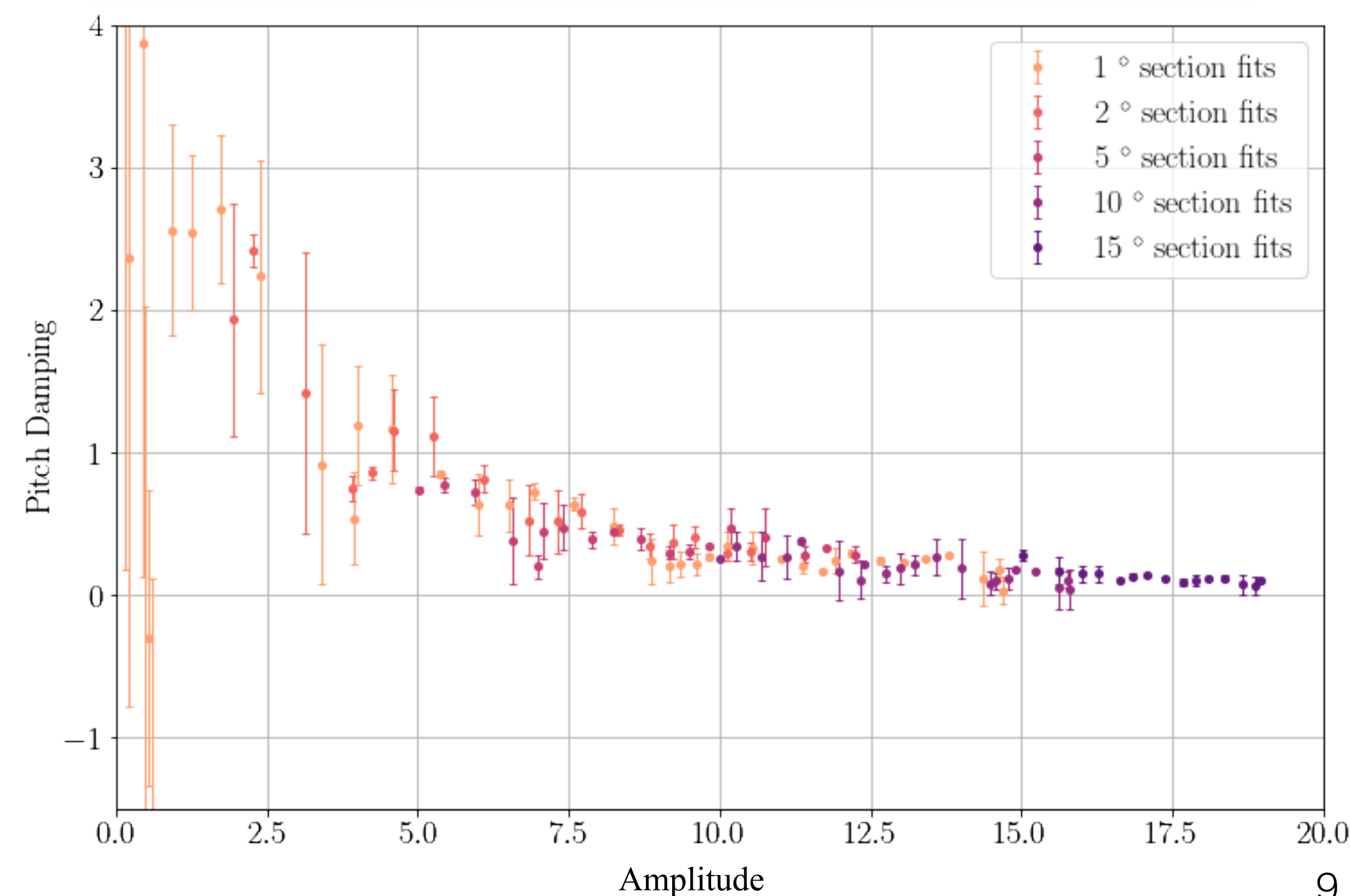
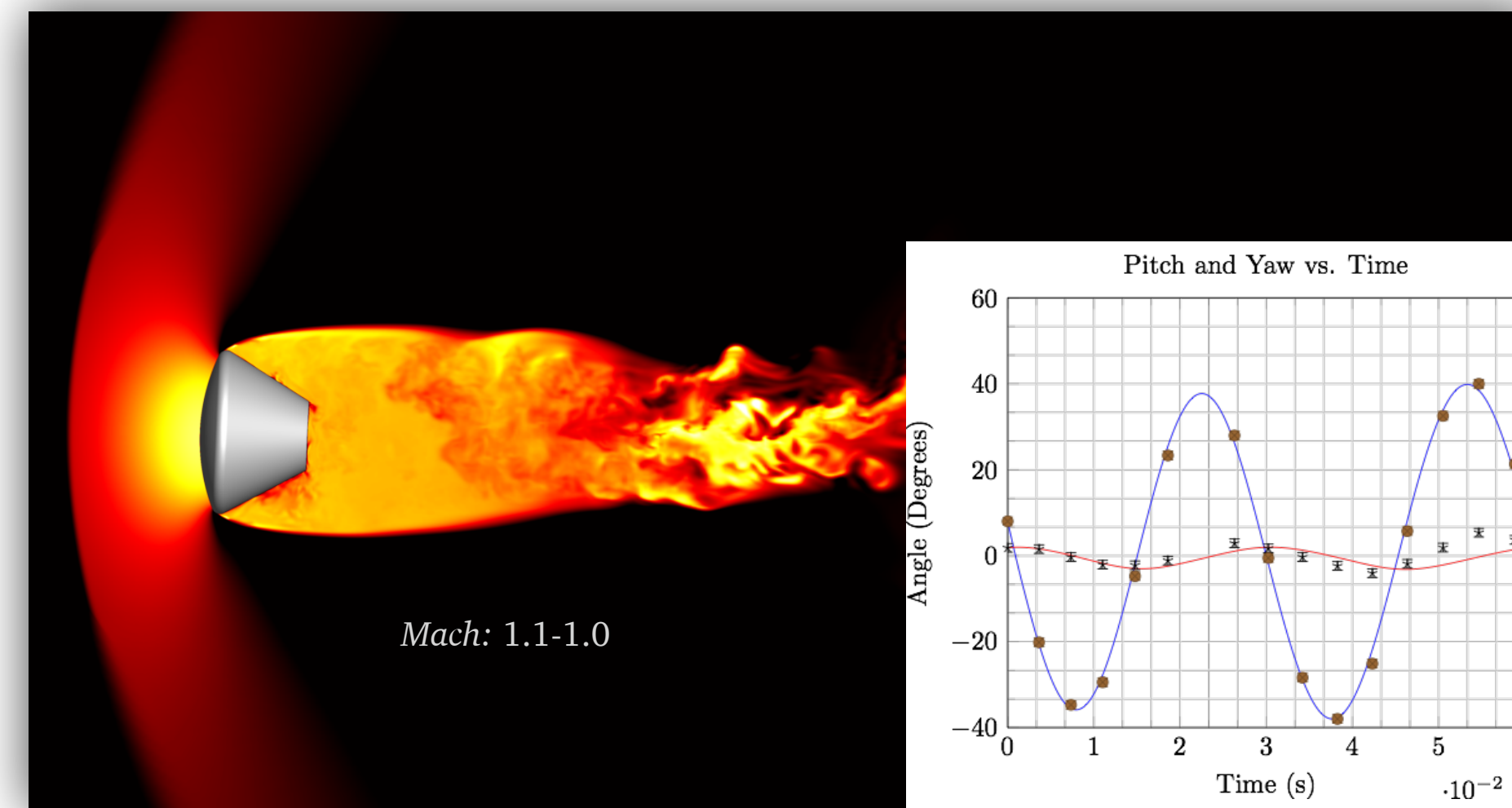
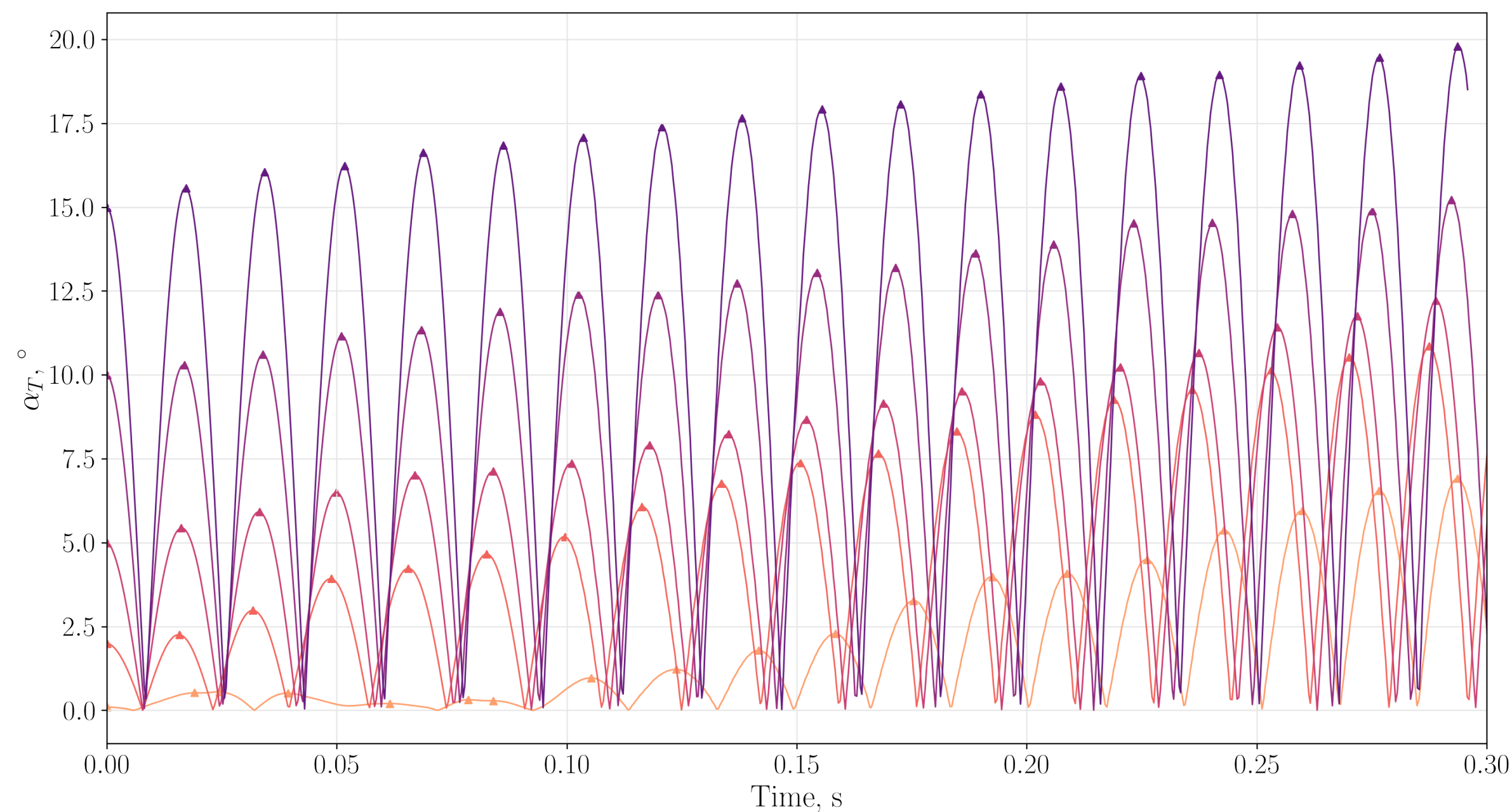
Results in a mapping across all *amplitudes*



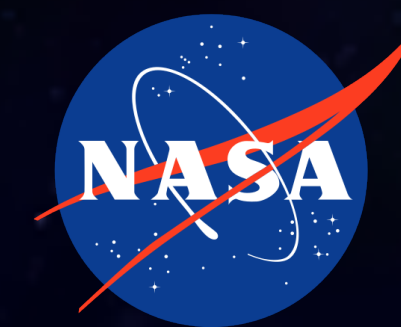
Comparison to Crew Module



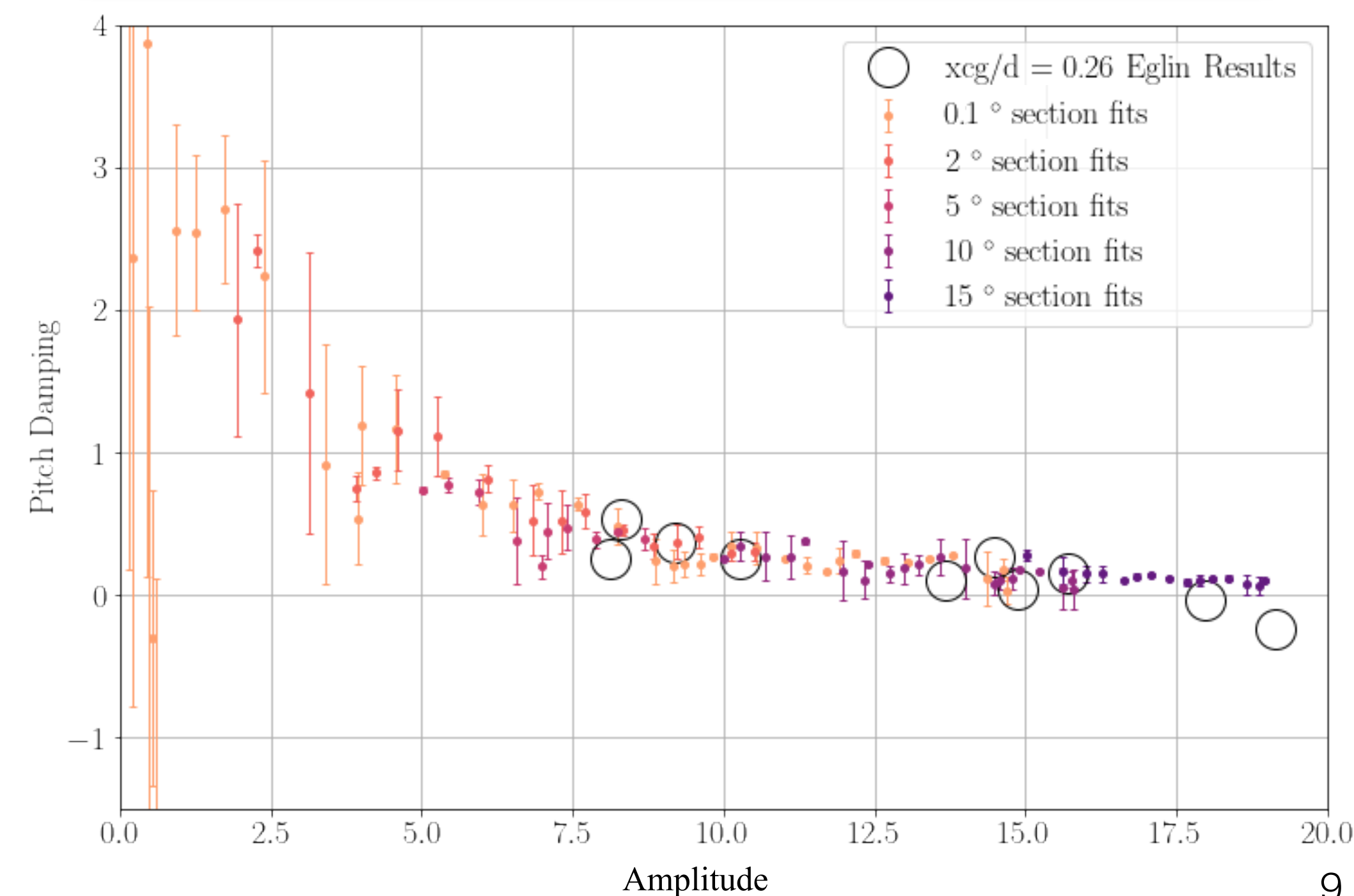
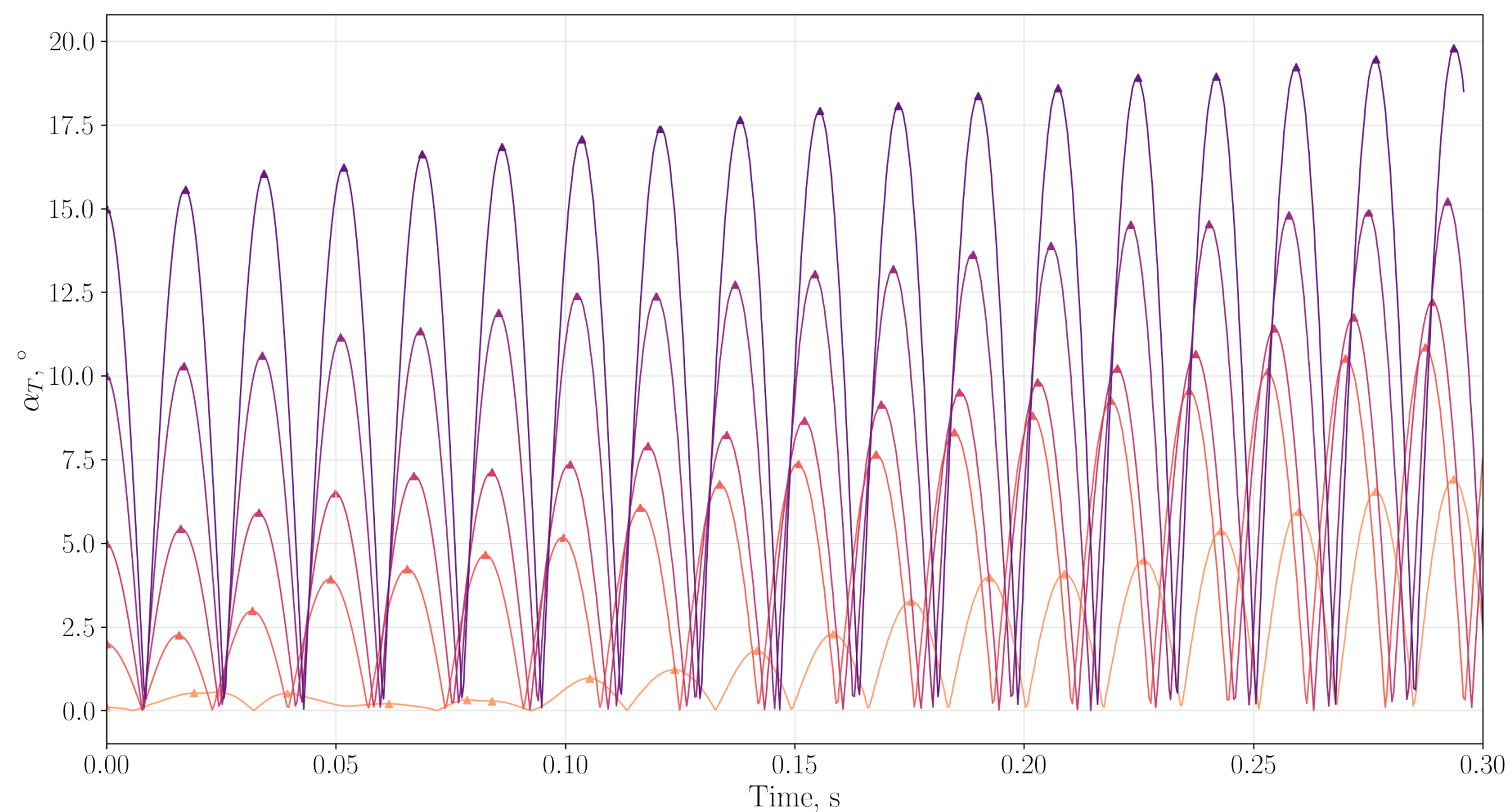
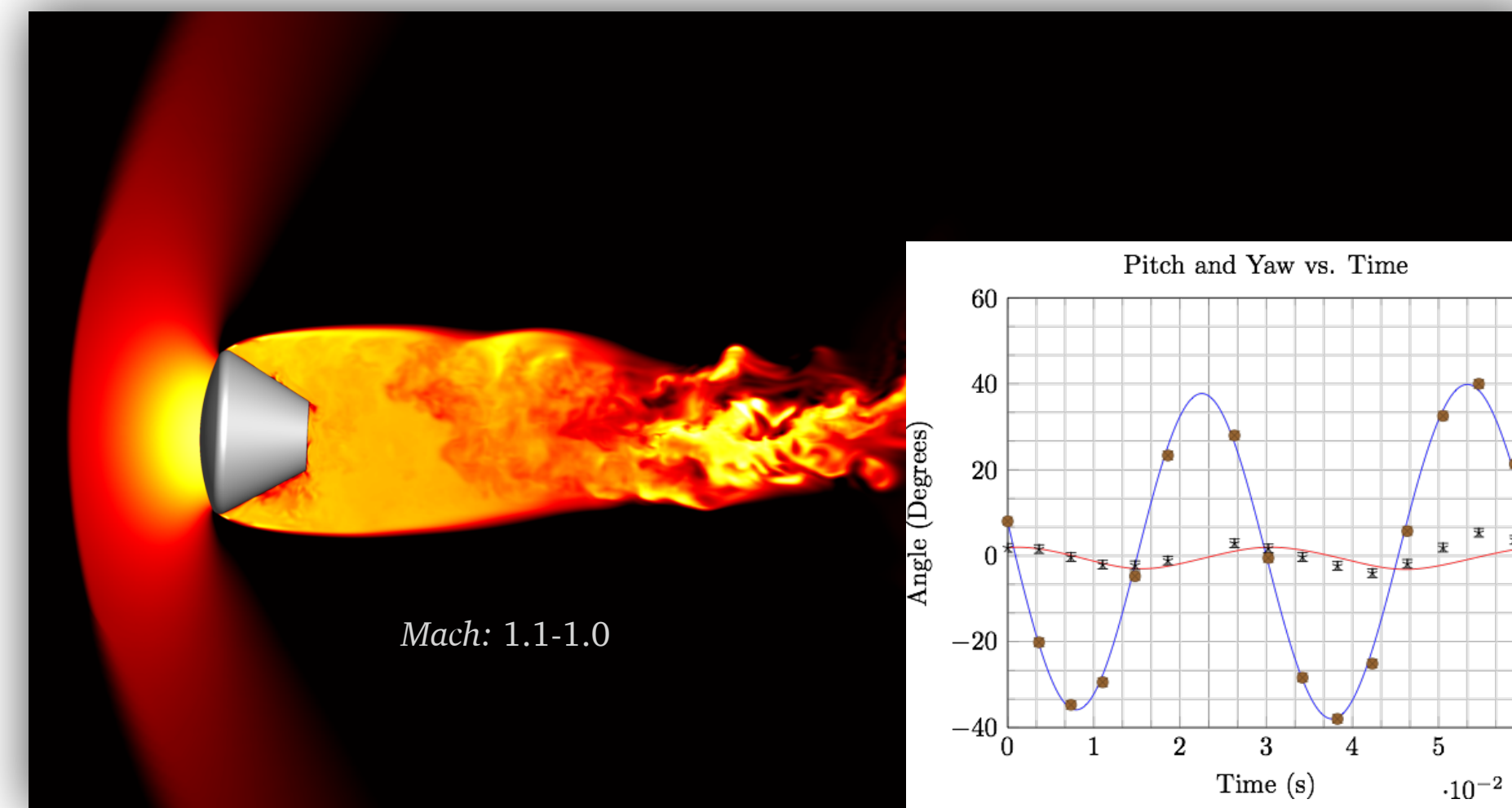
- 1-DoF FF-CFD dynamic analysis applied to Orion CM
 - Constant Mach=1.07 corresponding to mid Mach condition of HFFAF BR Shot 2366
- All initial amplitudes grow with no observable stable limit cycle
- Comparison of derived distribution of C_{m_q} section fits from 1-DoF trajectories agree well with experimental data obtained at a separate facility
 - Results suggest dynamic behavior is consistent between facility and simulation
- Static coefficients can be obtained from collection 1-DoF trajectories



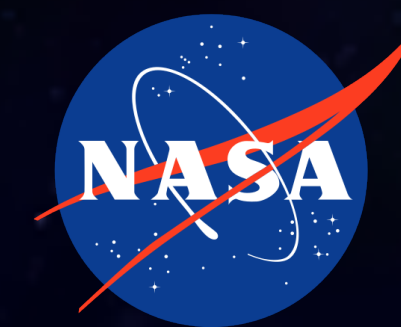
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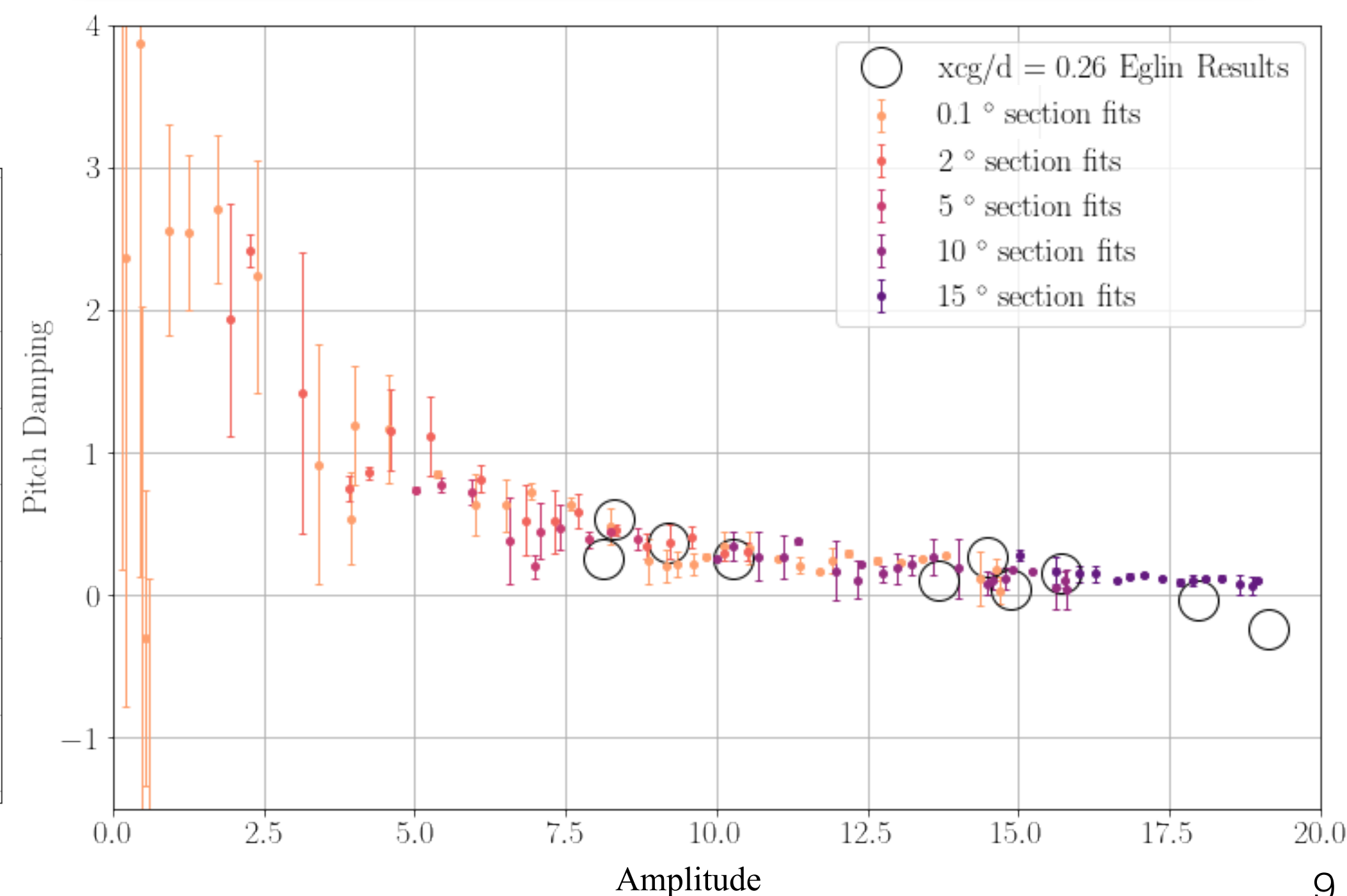
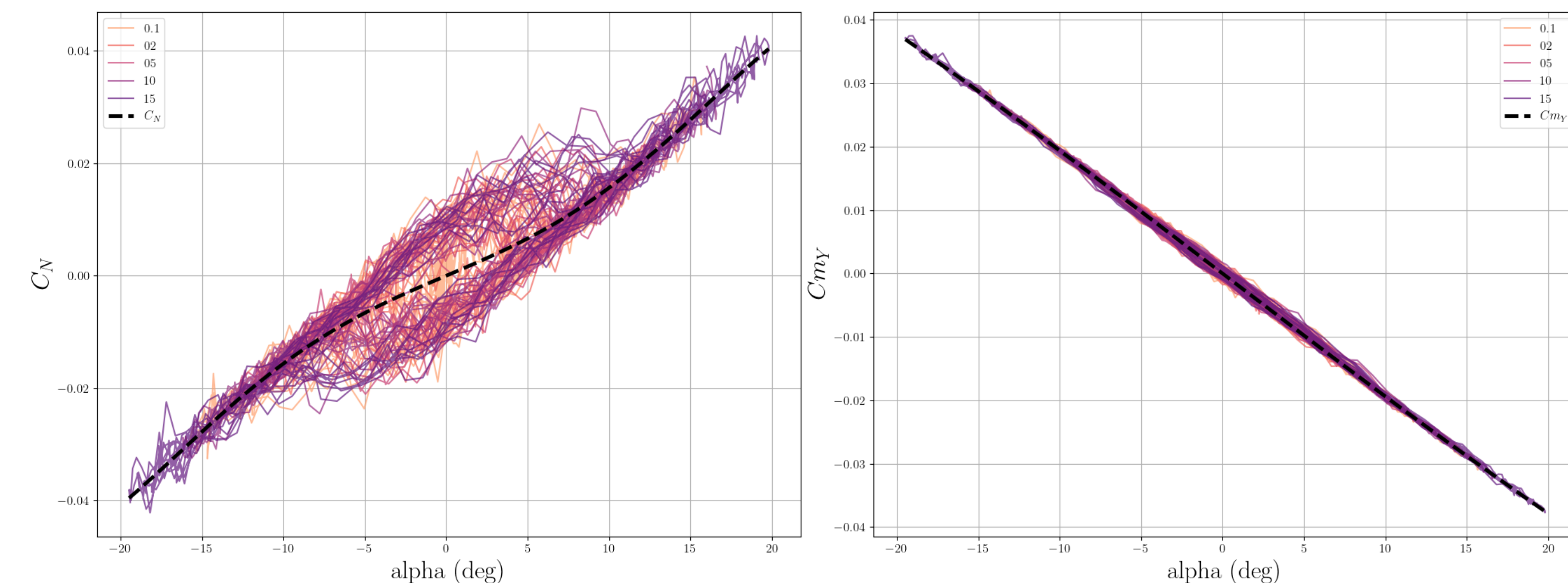
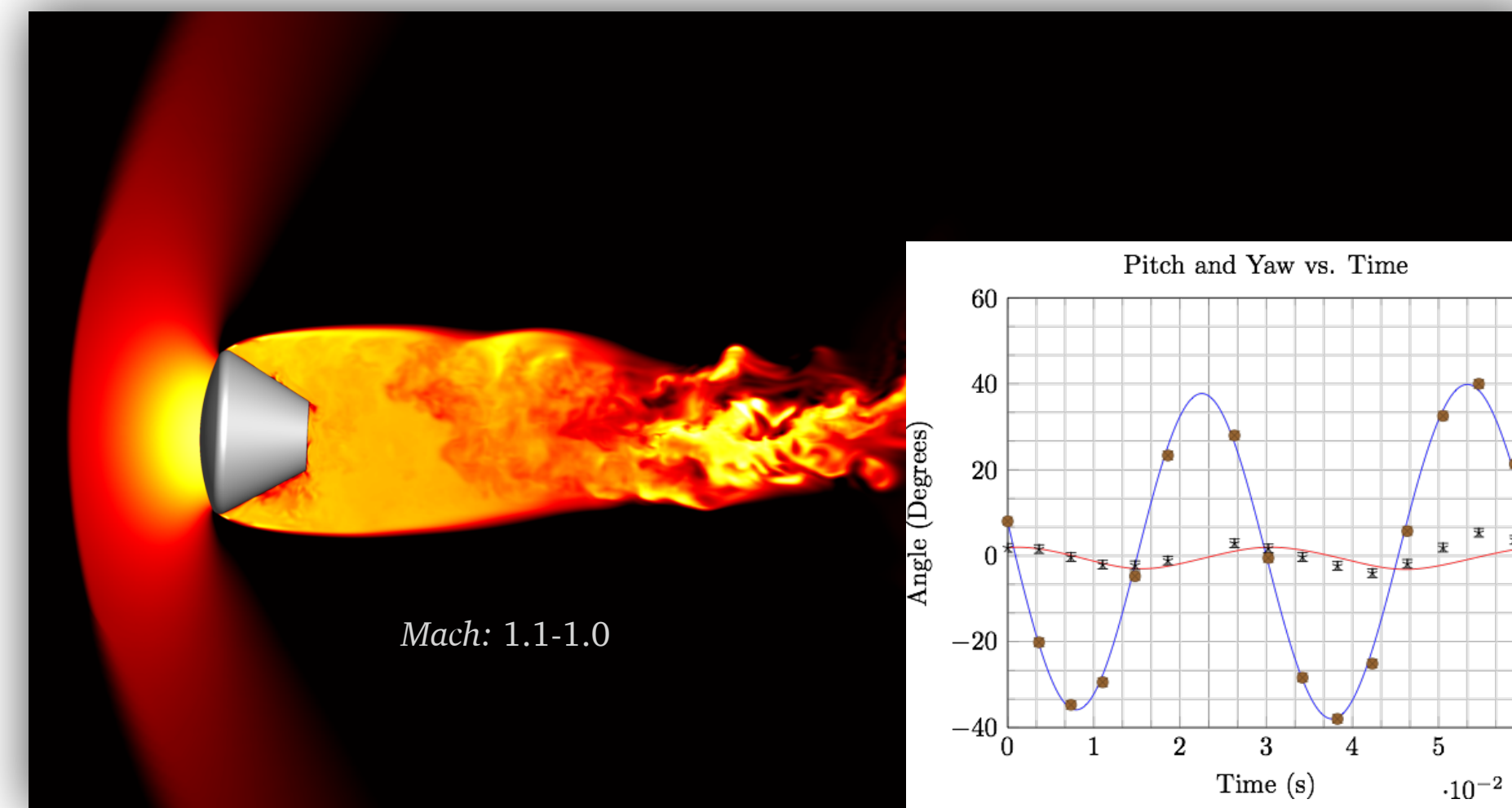
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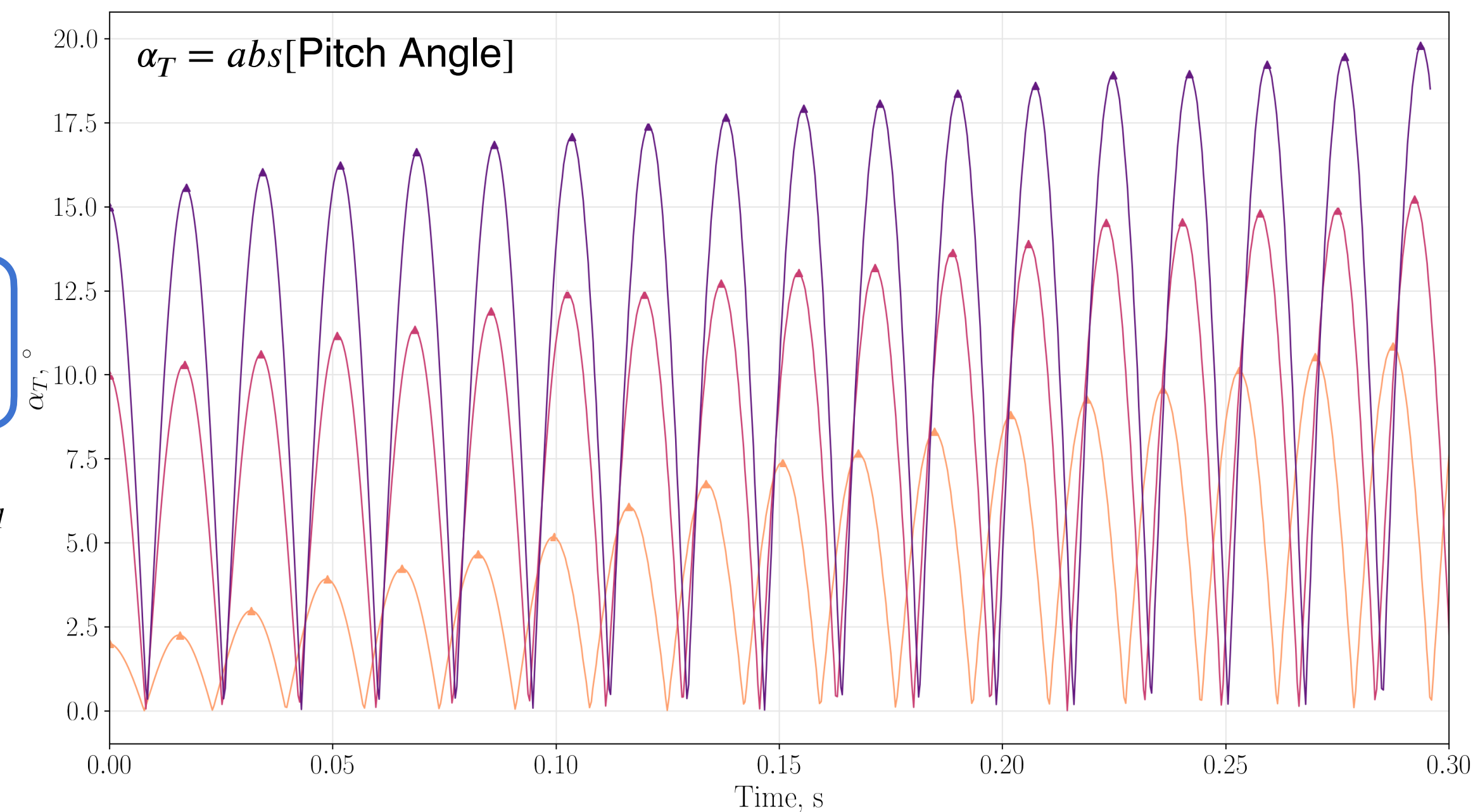
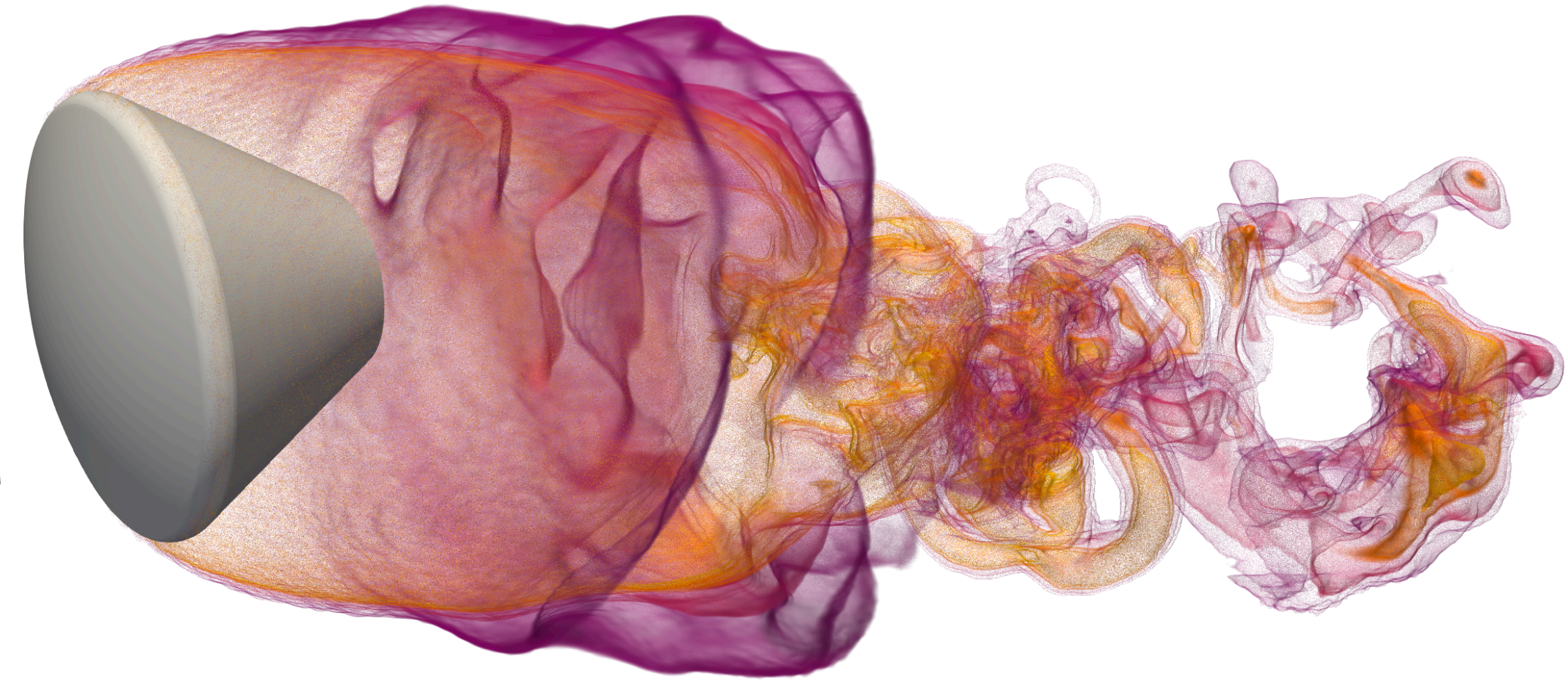
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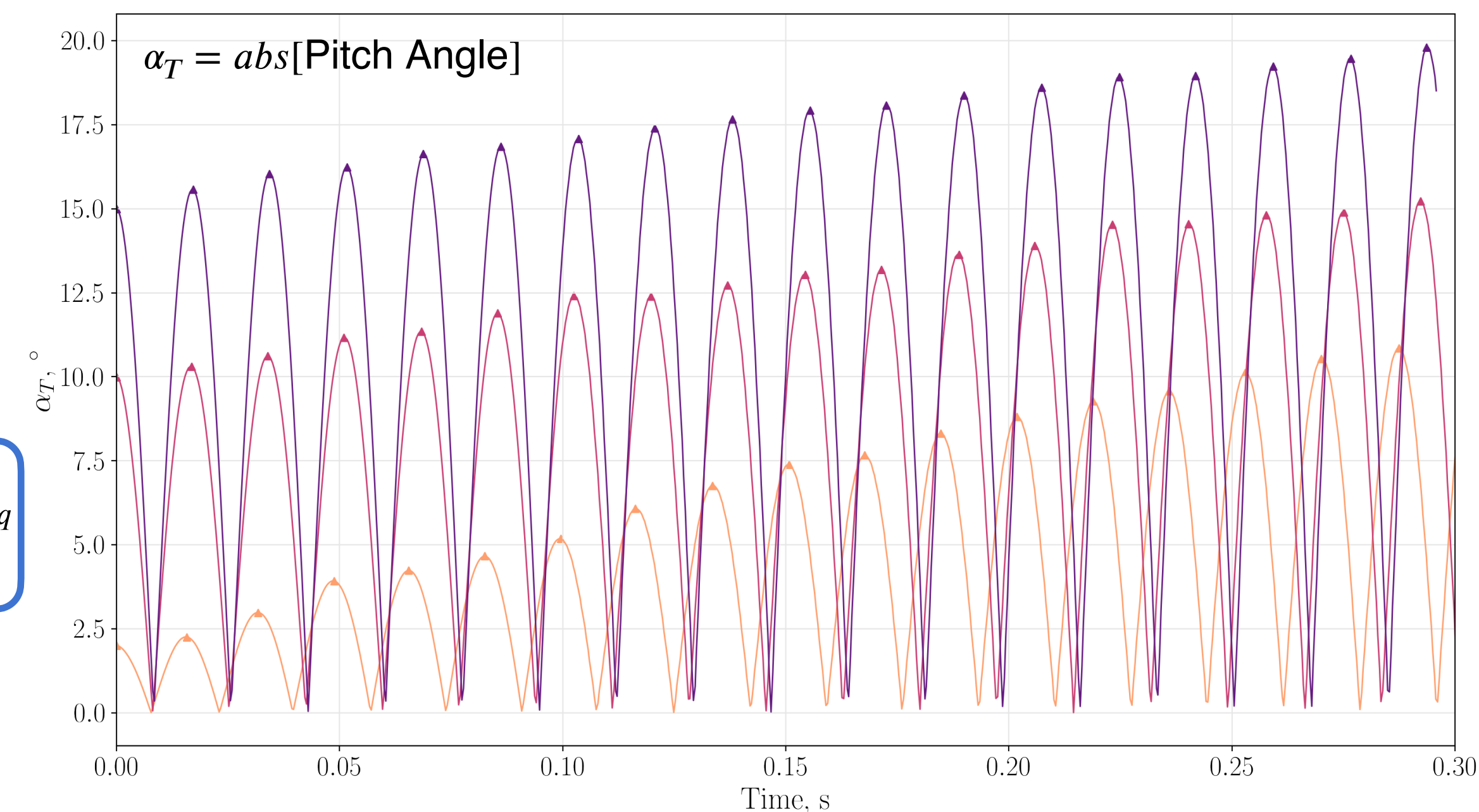
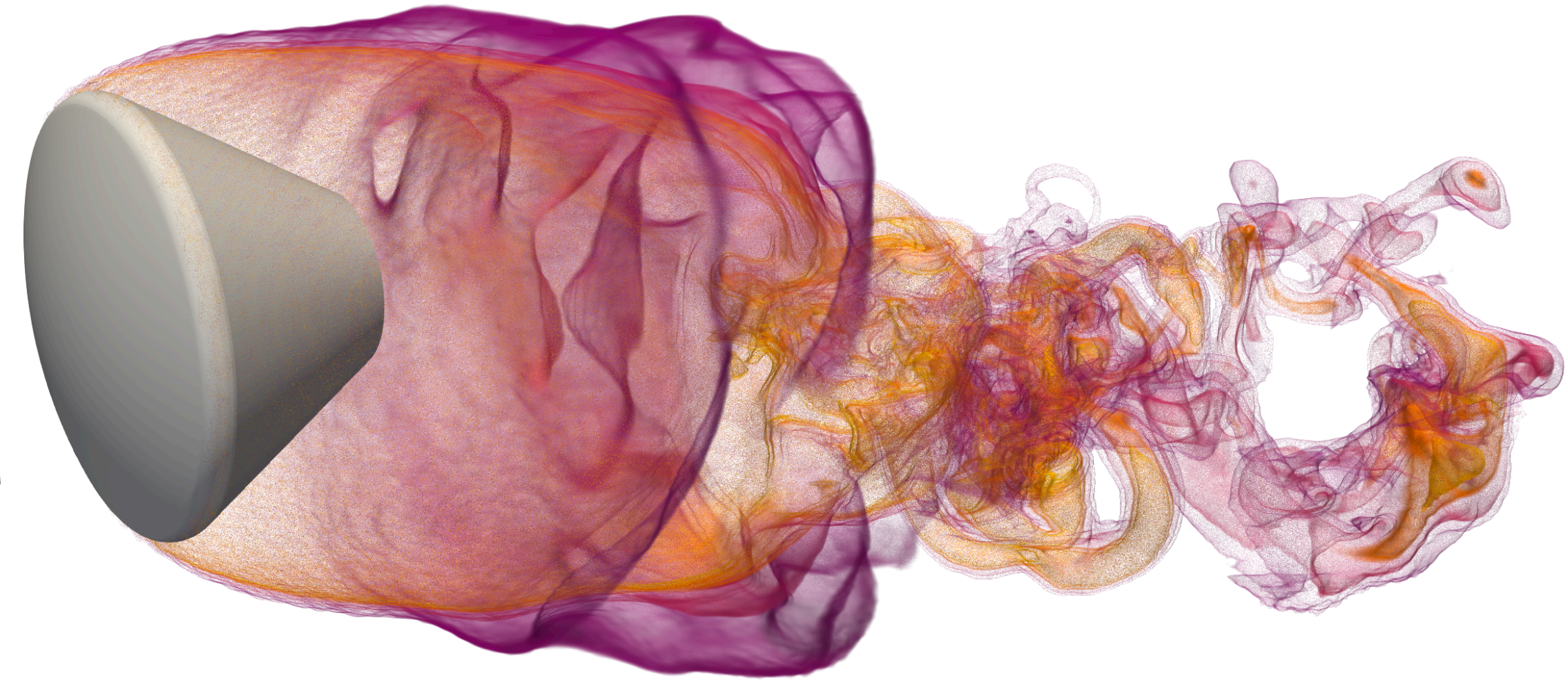
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 - A python suite of tools available to post-process FFCFD data and generate static and dynamic aero-coefficients
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- Two methods developed for using FF-CFD 1-DoF analysis to computing dynamic coefficients
 1. Run reduced 1DoF FF-CFD simulations and then:
 - 2a. Use analytical forms of equations to generate non-linear fits to C_{m_q} as a function of oscillation amplitude
 - 2b. Use inverse estimation and 1-DoF EOMs to identify optimal C_{m_q} curve as a function of instantaneous angle of attack.



Inverse Estimation of Pitch Damping at Constant Mach (1-DoF)

End-to-End pipeline has been created for extracting static and dynamic aero coefficients from 1-DoF (free-to-pitch) FF-CFD simulations

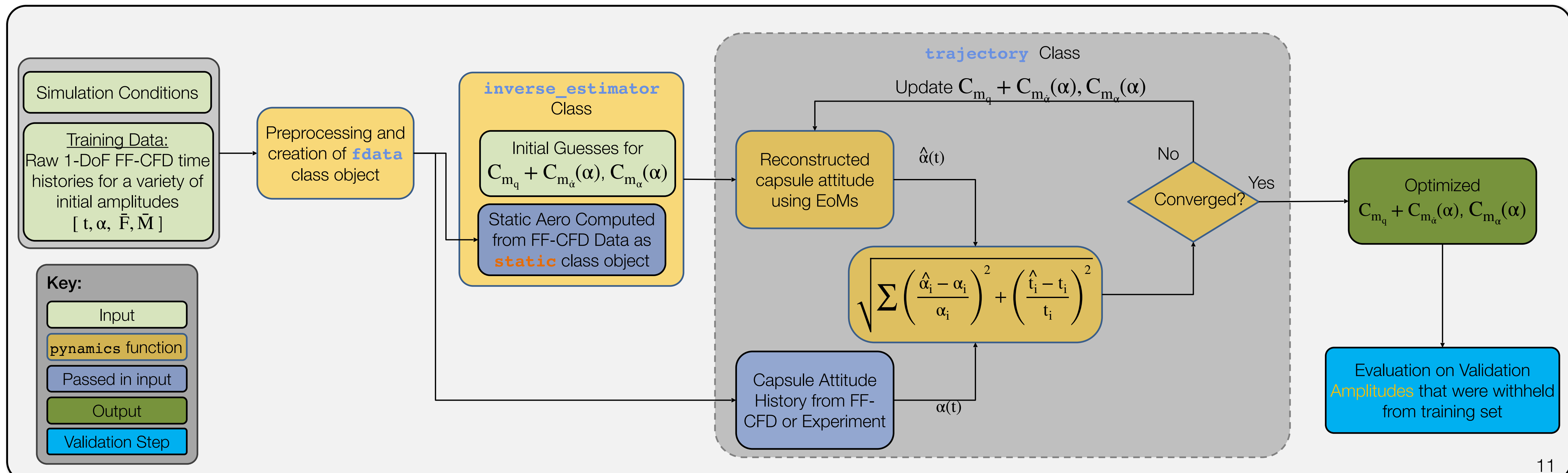
- Theory suggests and previous work has shown that pitch damping coefficient derived from 1-DoF is equivalent to that from higher DoF simulations

• Reconstruction: Using the ODE derived by Schoenenberger, Queen:
$$\ddot{\alpha} - \frac{\rho VS}{2m} \left(-C_{L_\alpha} + \frac{md^2}{2I} (C_{m_q} + C_{m_{\dot{\alpha}}}) \right) \dot{\alpha} - \frac{\rho V^2 S d}{2I} C_{m_\alpha} \alpha = 0$$
 integrate forwards in time using Python's **solve_ivp** to generate a trajectory history

– Requires: dof simplifications, geometric constants, static aero coefficients, α_0 (initial amplitude), $\dot{\alpha}_0$ (local maxima), and $C_{m_q} + C_{m_{\dot{\alpha}}}$ as a function of α

- Optimization: Send Python's **scipy.optimize.minimize** a functional form of the pitch damping curve with an initial guess, wrap the reconstruction (**solve_ivp**) scheme in the optimizer, and iterate on input curve coefficients to **minimize the normalized L₂ residual between peak amplitudes**

– Optional inclusion of peak times in the objective function allows for co-optimization of C_{m_α} (shown below). Otherwise, compute in static aero routine.



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Training Data at Various Machs:

Mach 0.6 [1°, 2°, 5°, 10°, 20°, 30°]
Mach 1.1 [1°, 2°, 5°, 10°, 20°, 30°]
Mach 1.5 [1°, 2°, 5°, 10°, 20°, 30°]
Mach 2.0 [1°, 2°, 5°, 10°, 20°, 30°]
Mach 3.0 [1°, 2°, 5°, 10°, 20°, 30°]

Key:

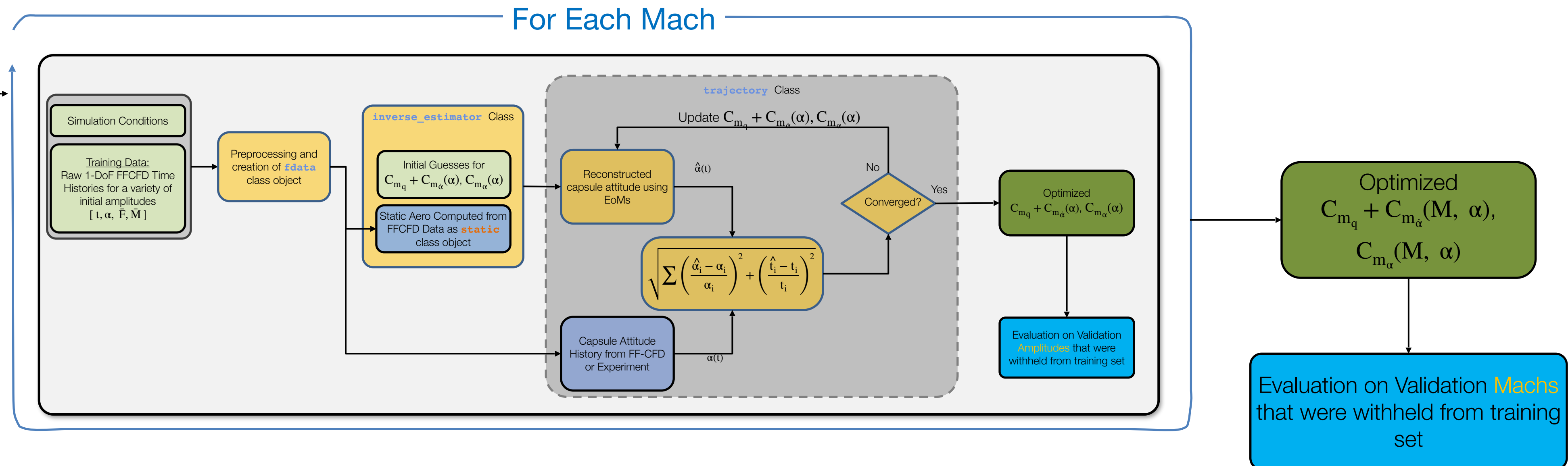
Input

pynamics function

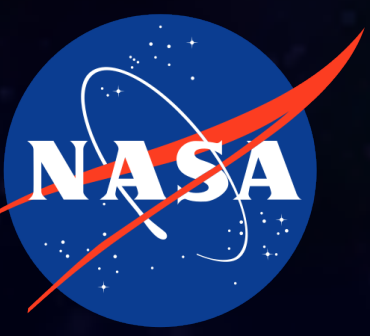
Passed in input

Output

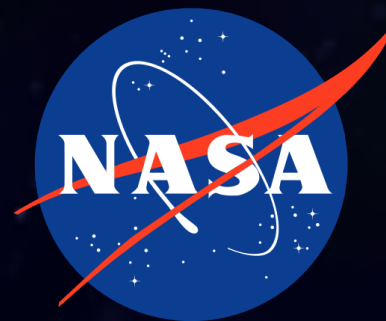
Validation Step



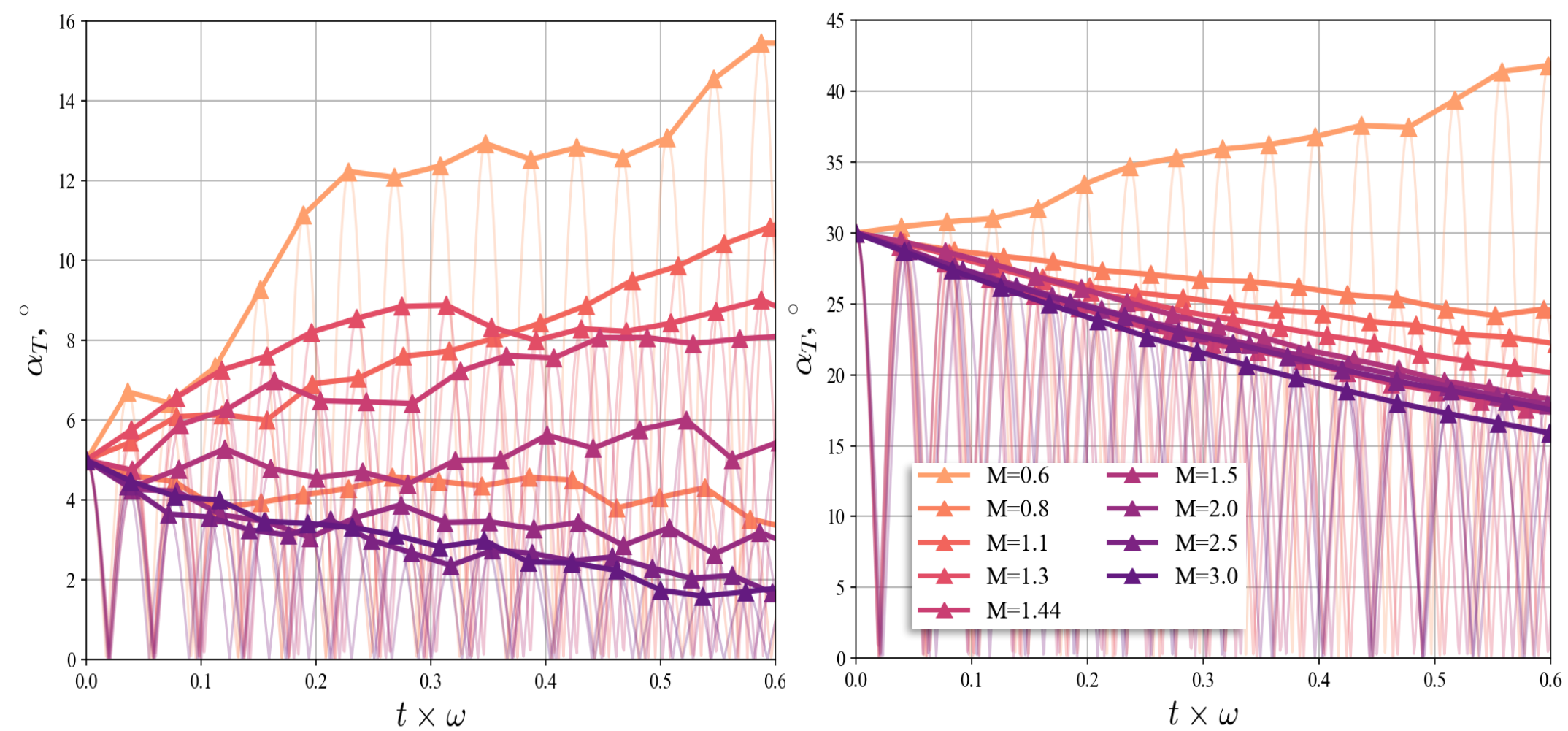
End-to-End Example



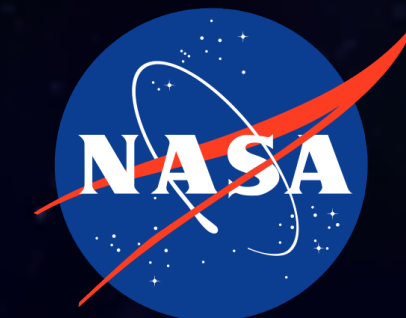
End-to-End Example



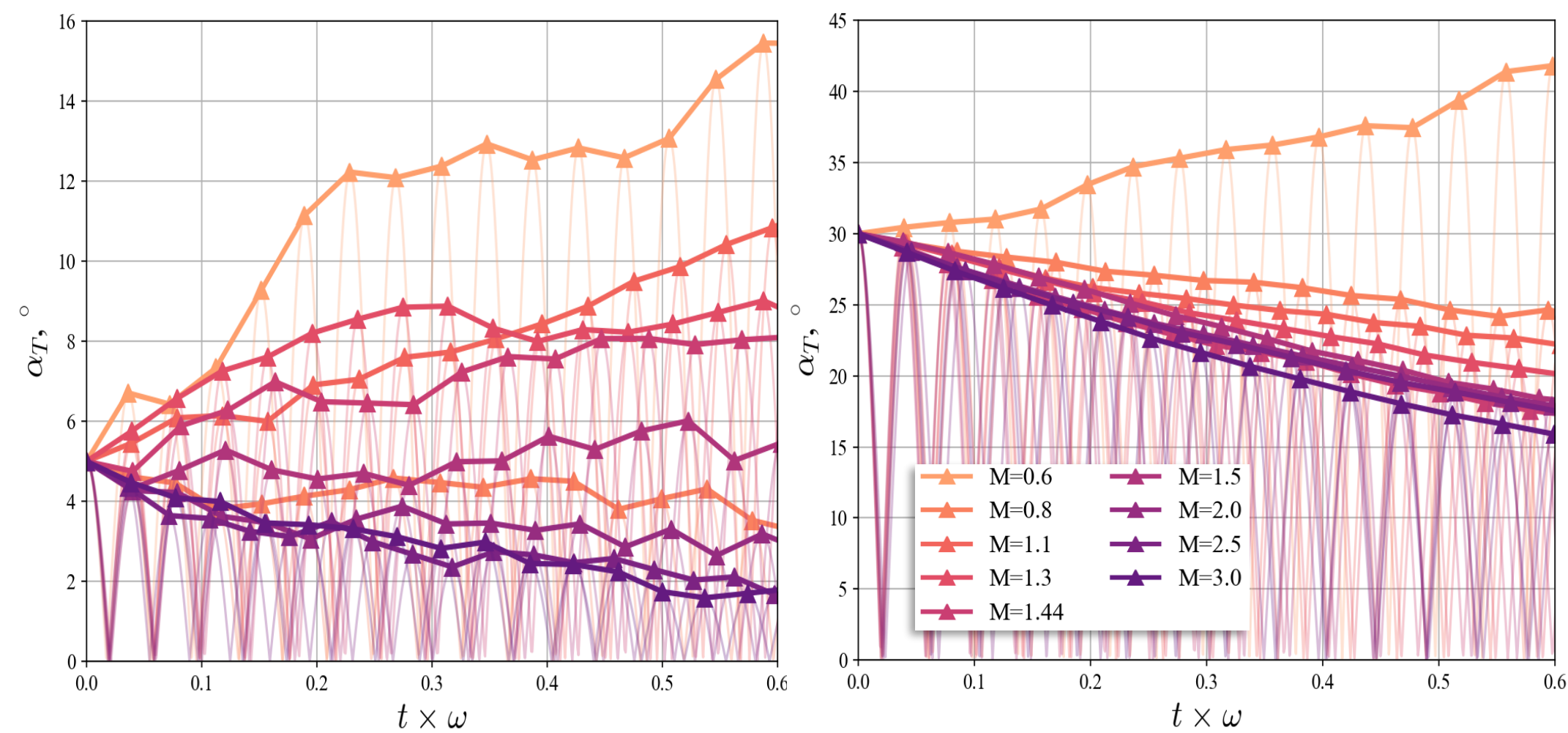
Complete FFCFD Data Set



End-to-End Example

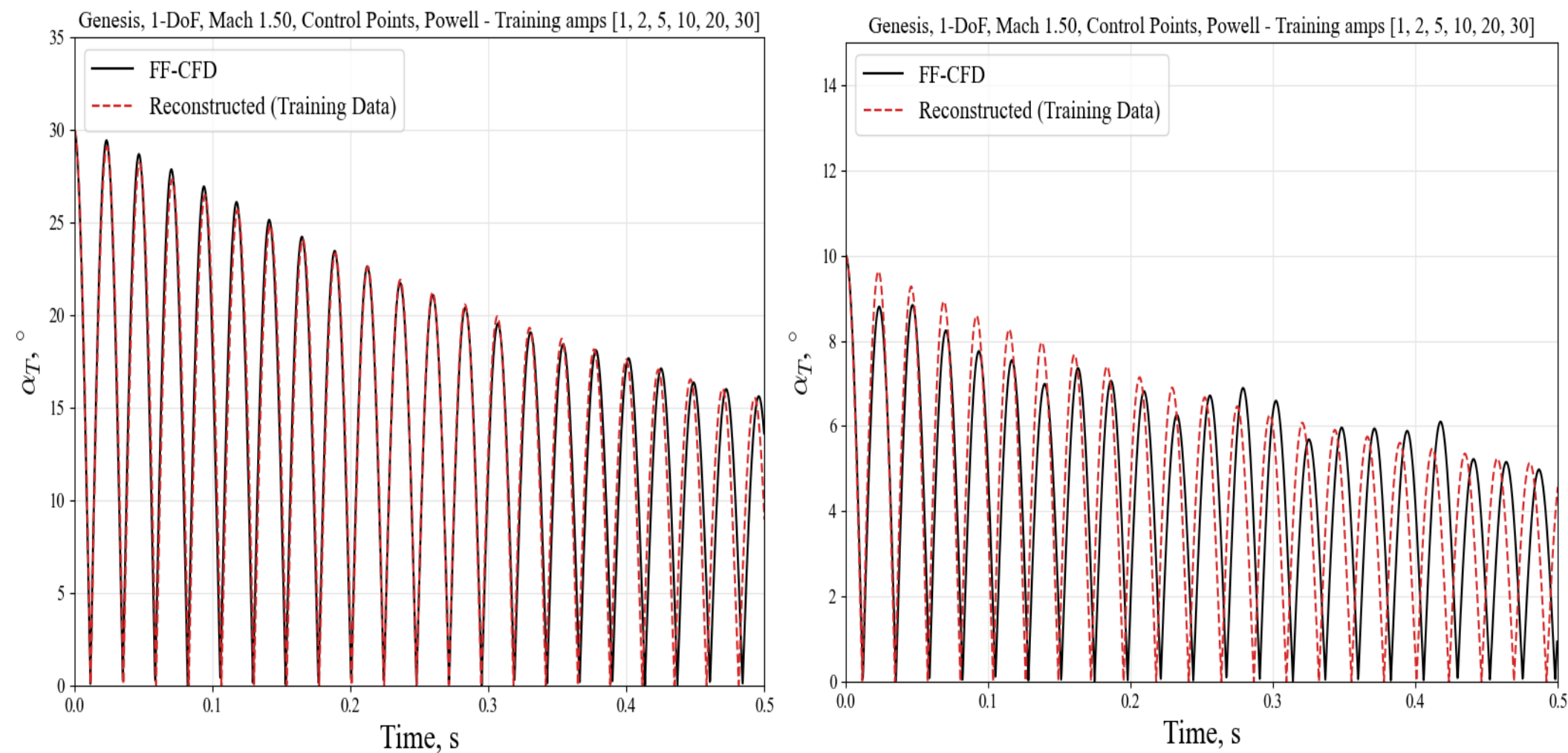


Complete FFCFD Data Set

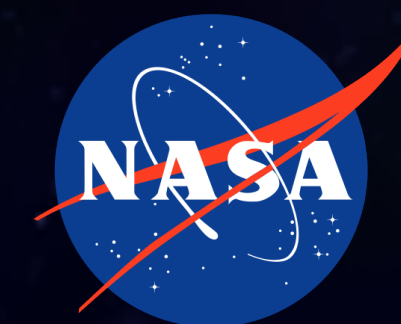


Train

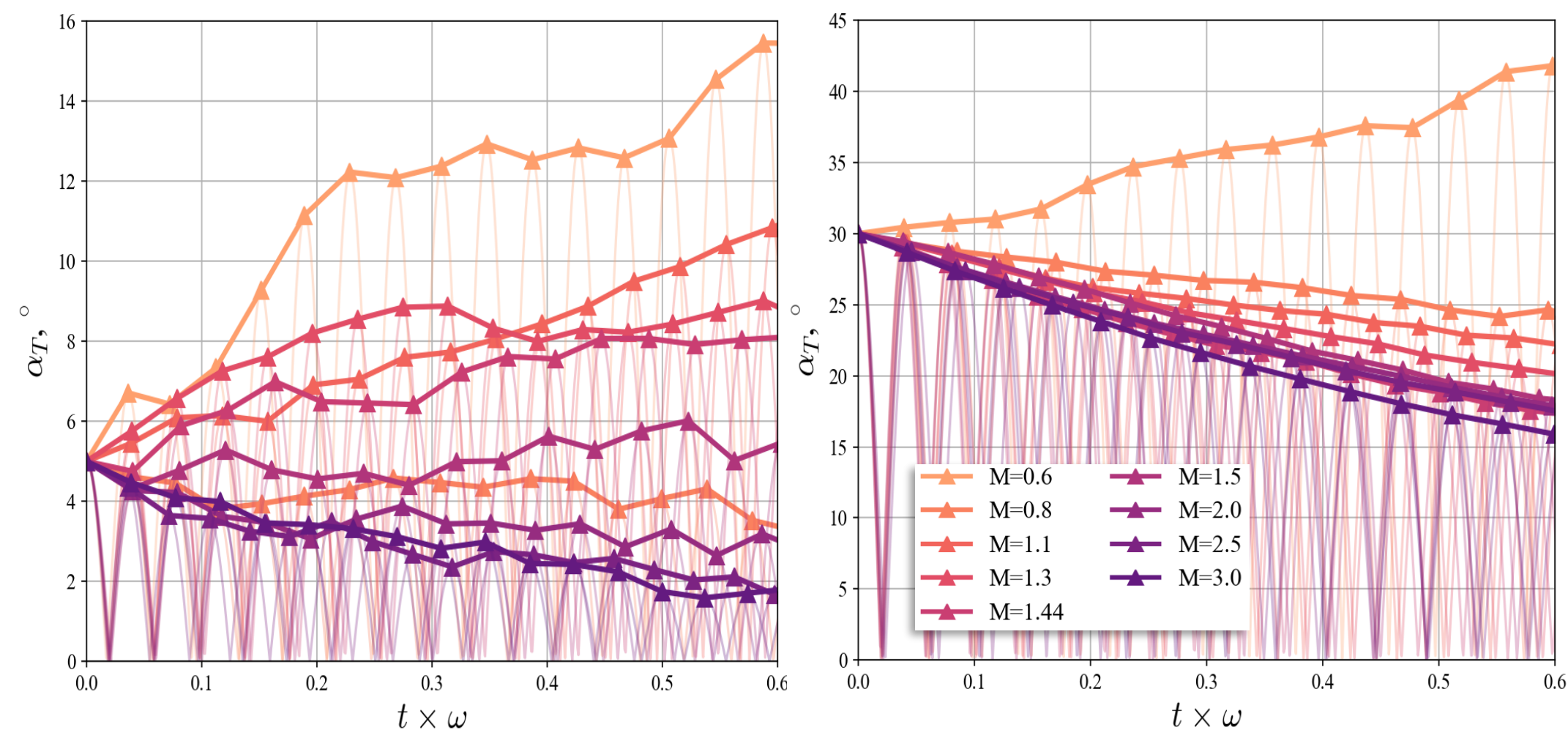
Model Fit Performance
on Training Data (M1.5)



End-to-End Example

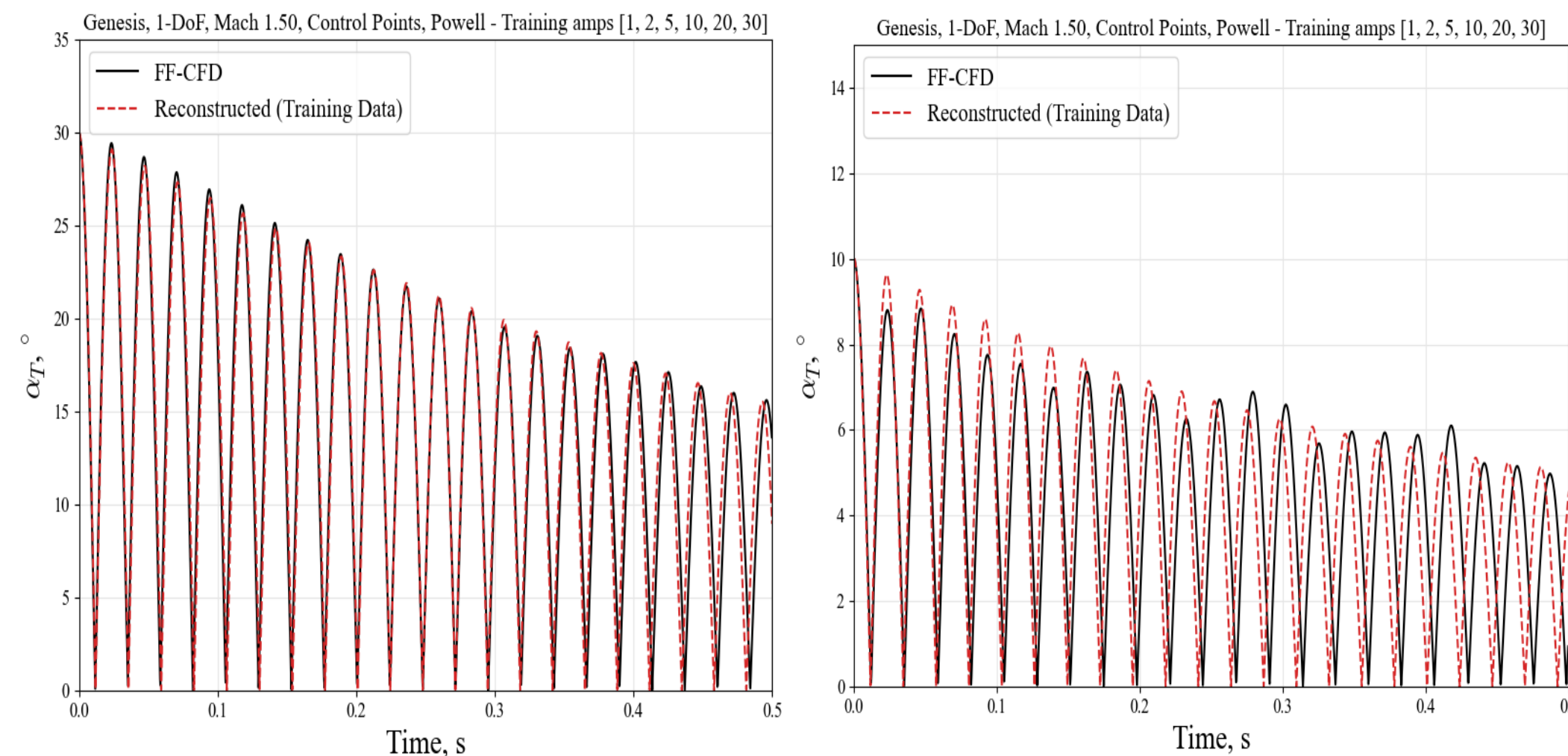


Complete FFCFD Data Set



Train

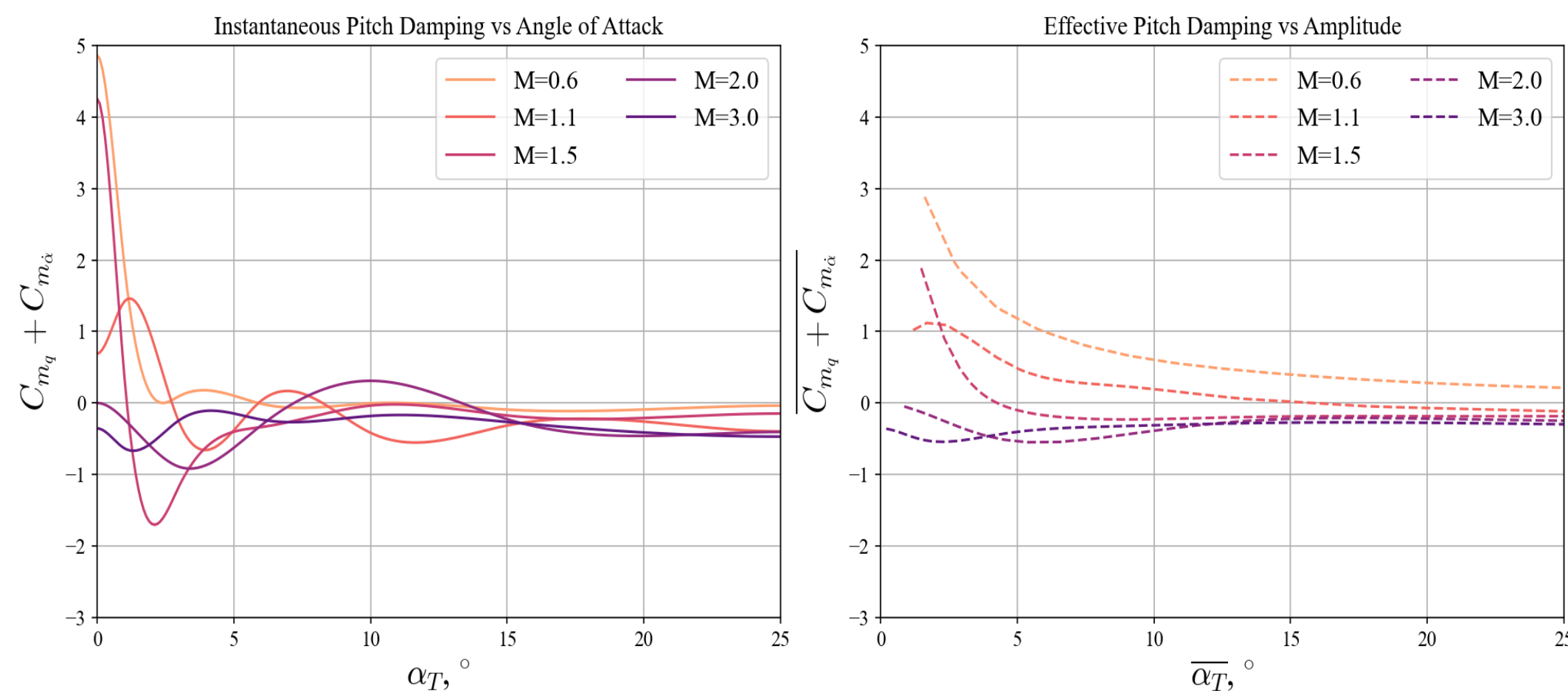
Model Fit Performance
on Training Data (M1.5)



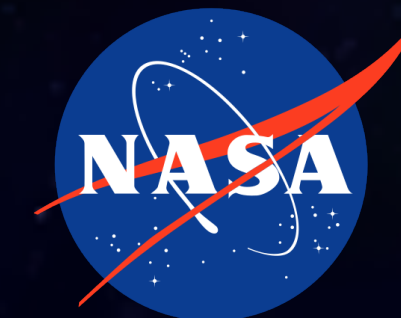
$C_{m_q}(M, \alpha)$

Genesis FFCFD Aerodatabase Generated using Mach 0.6, 1.1, 1.5 2.0, & 3.0

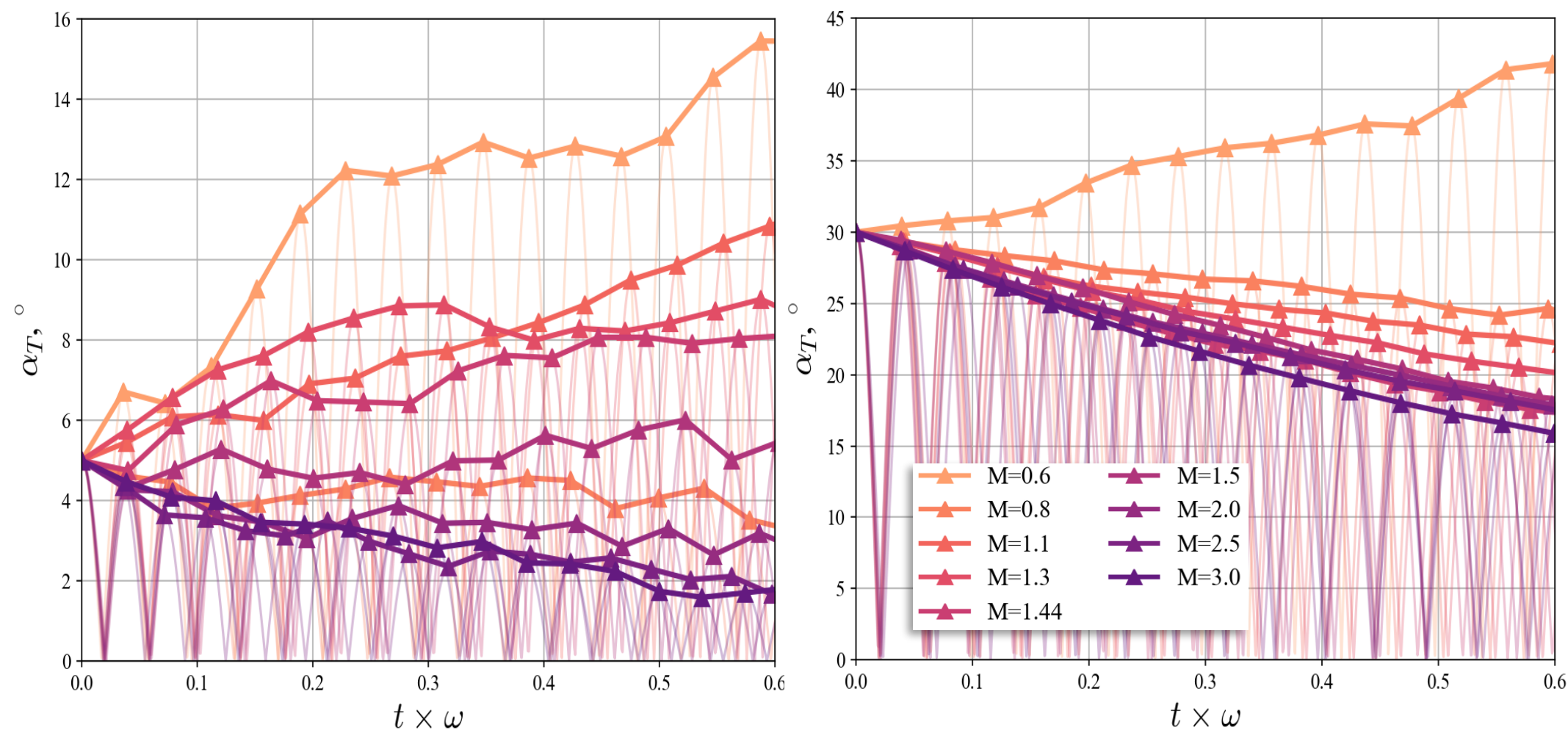
Static and Dynamic
Aerodatabase as $f(M, \alpha)$



End-to-End Example

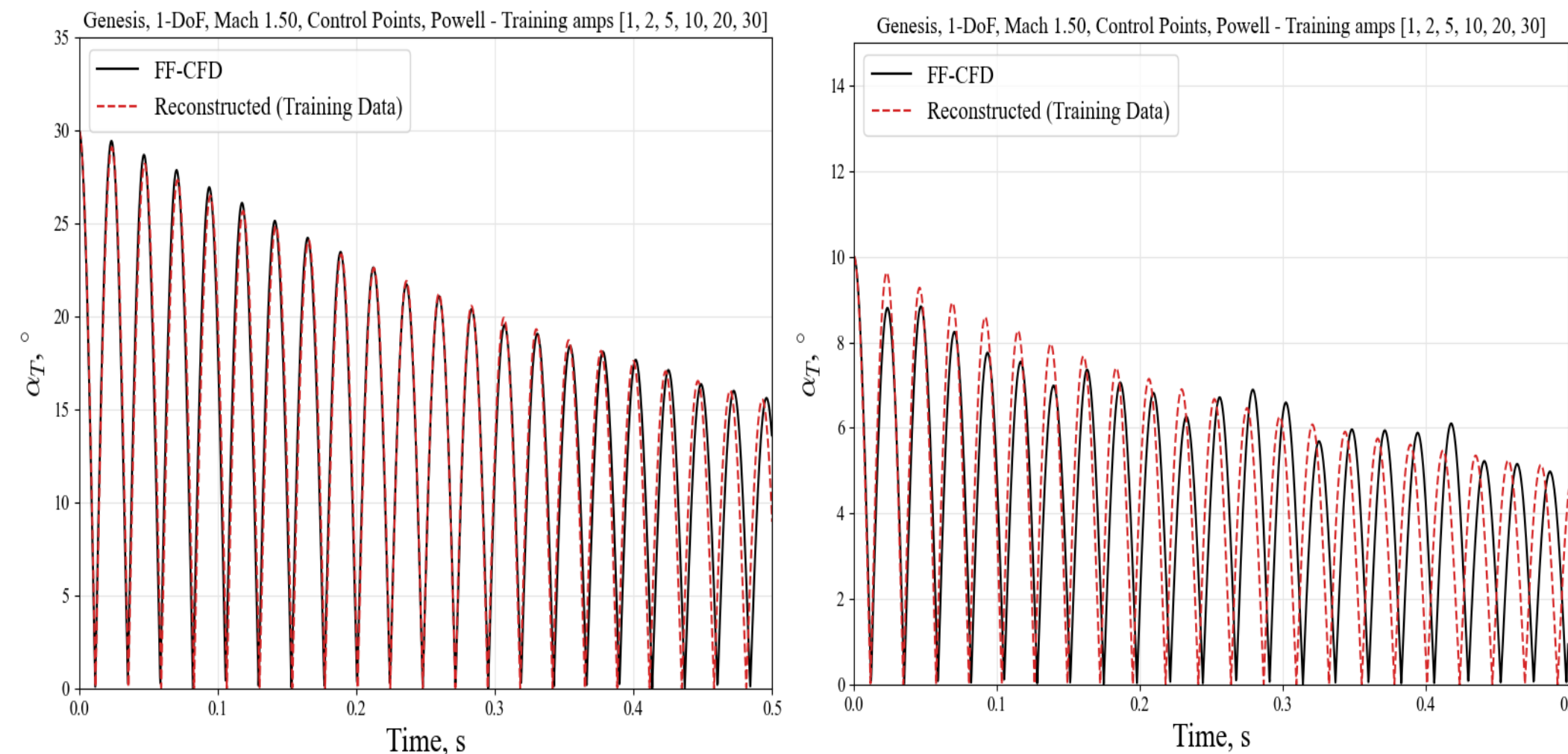


Complete FFCFD Data Set



Train

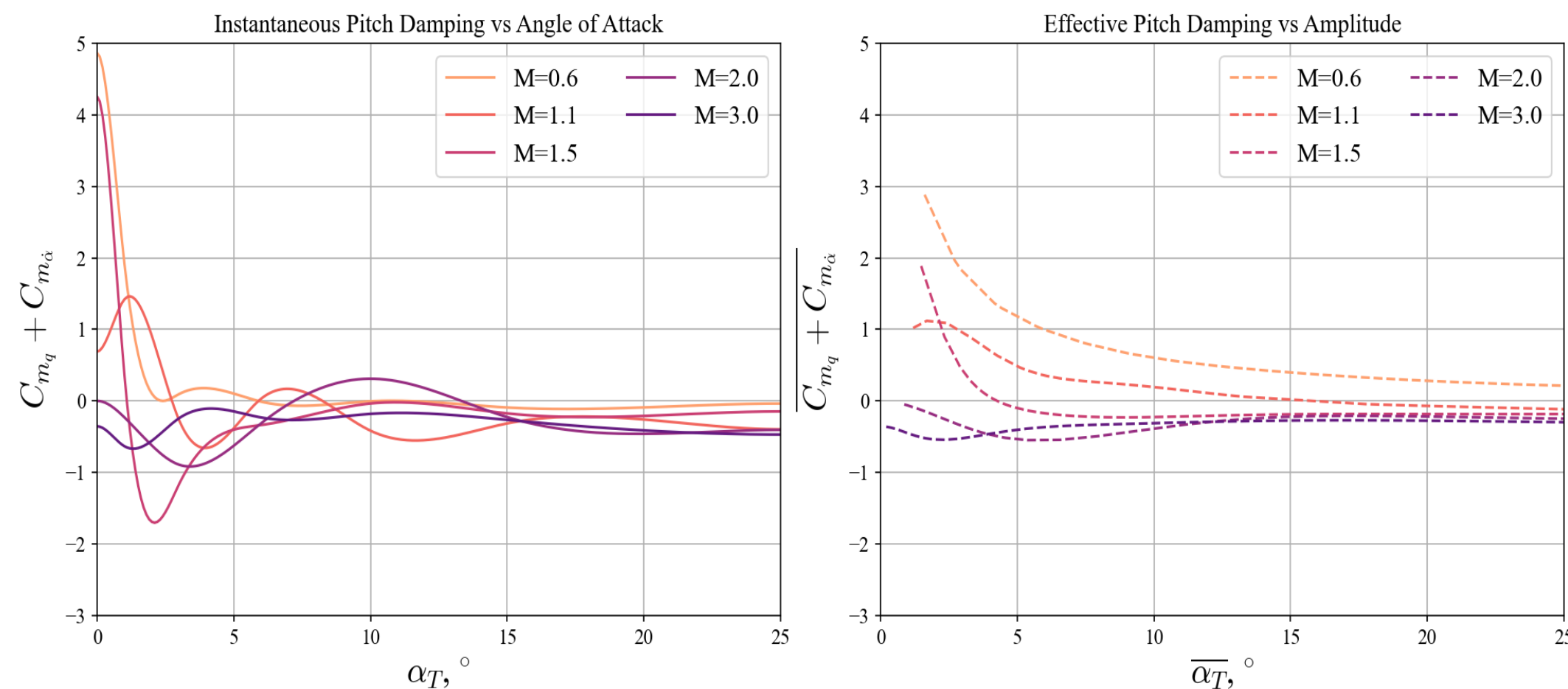
Model Fit Performance
on Training Data (M1.5)



$C_{m_q}(M, \alpha)$

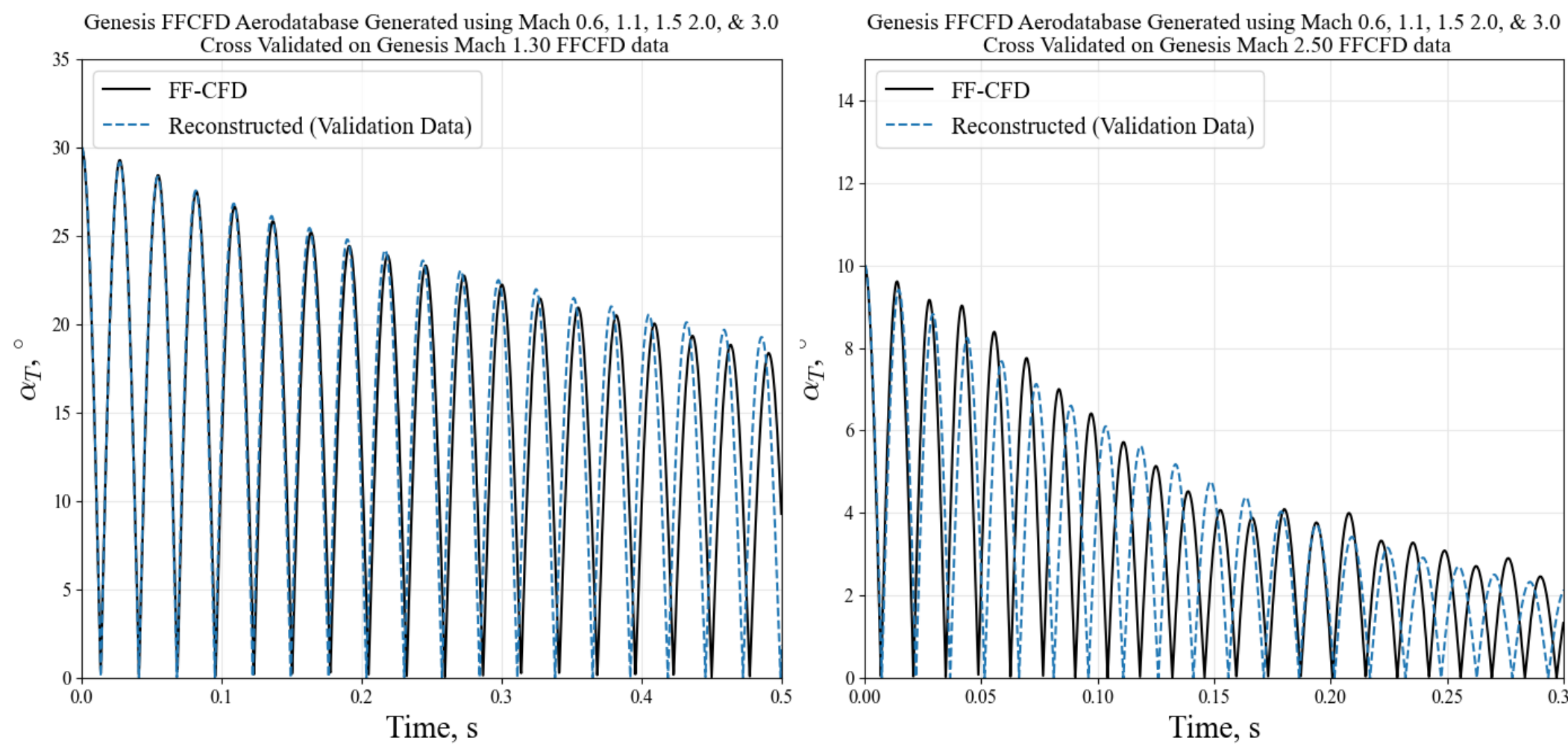
Genesis FFCFD Aerodatabase Generated using Mach 0.6, 1.1, 1.5 2.0, & 3.0

Static and Dynamic
Aerodatabase as $f(M, \alpha)$



Validate

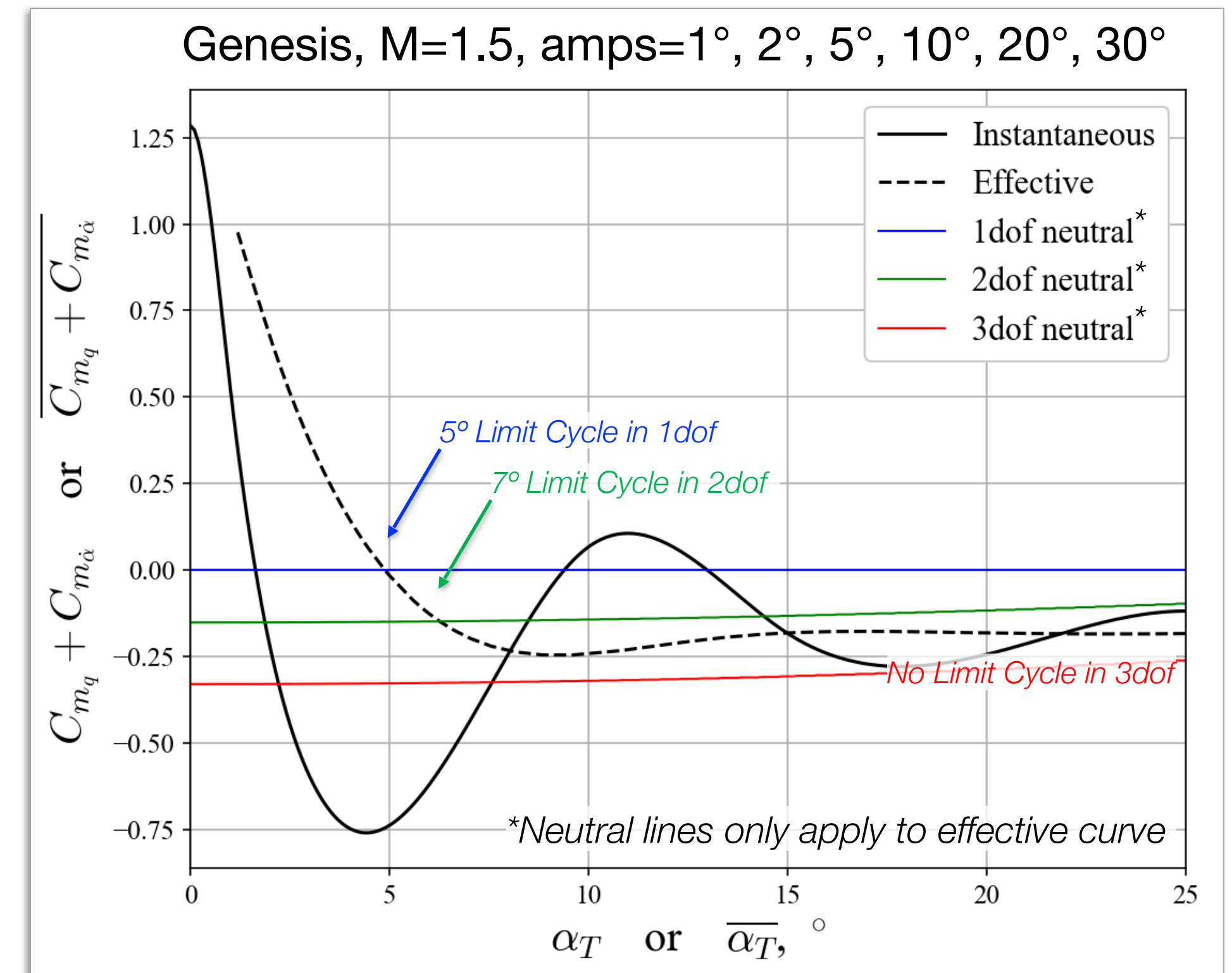
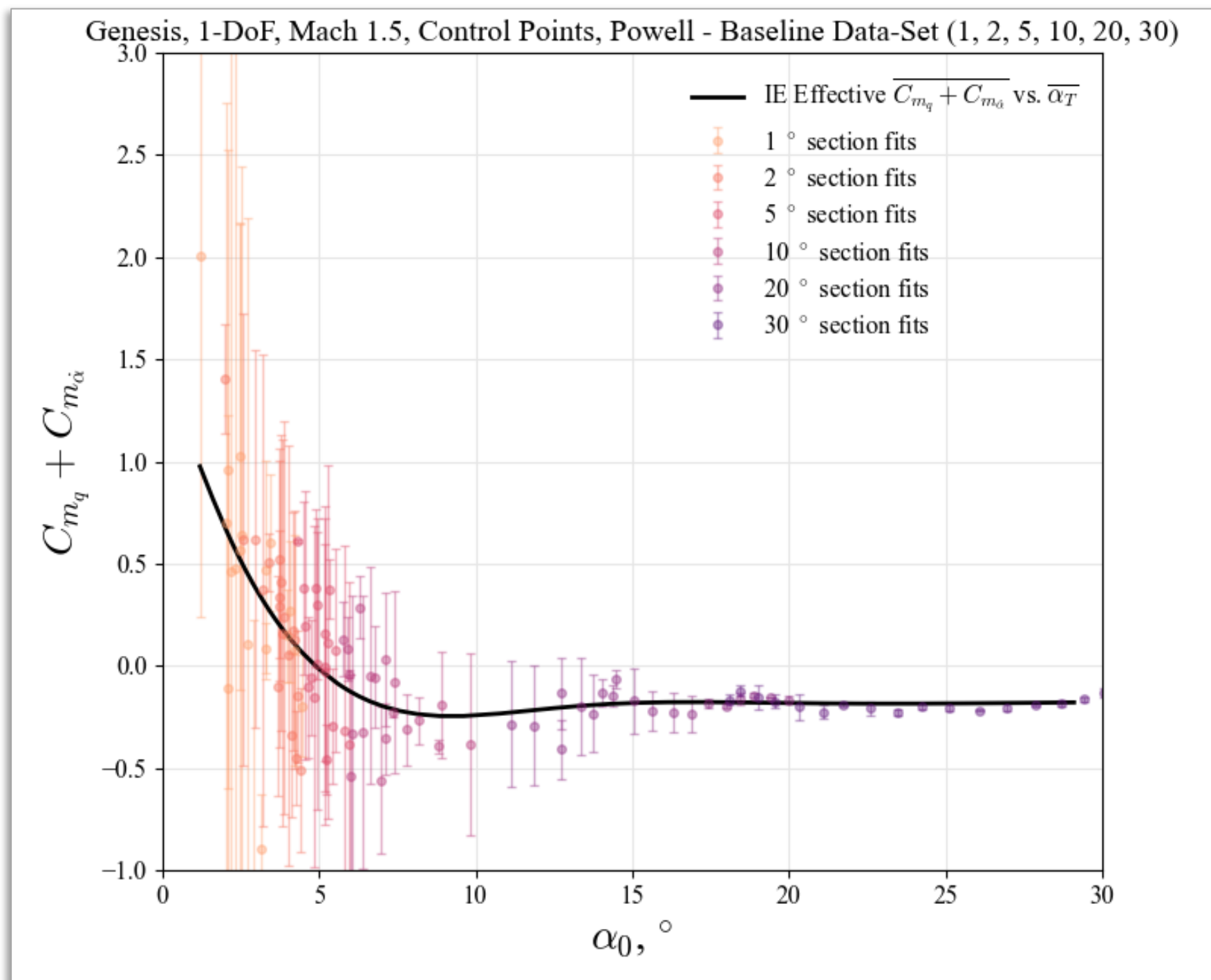
Model Validation on previously
unseen Data (M1.3 and 2.5)



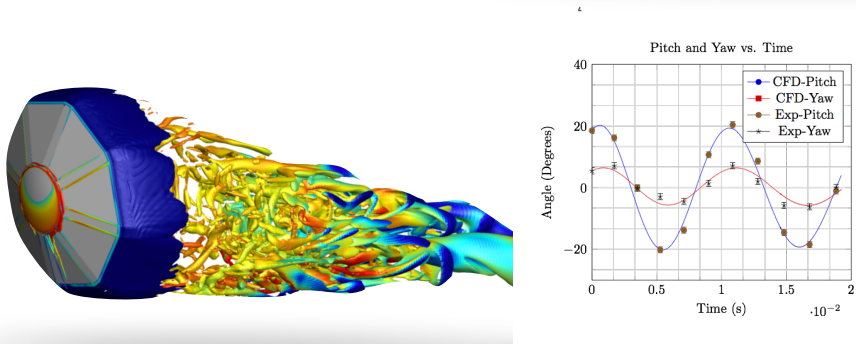
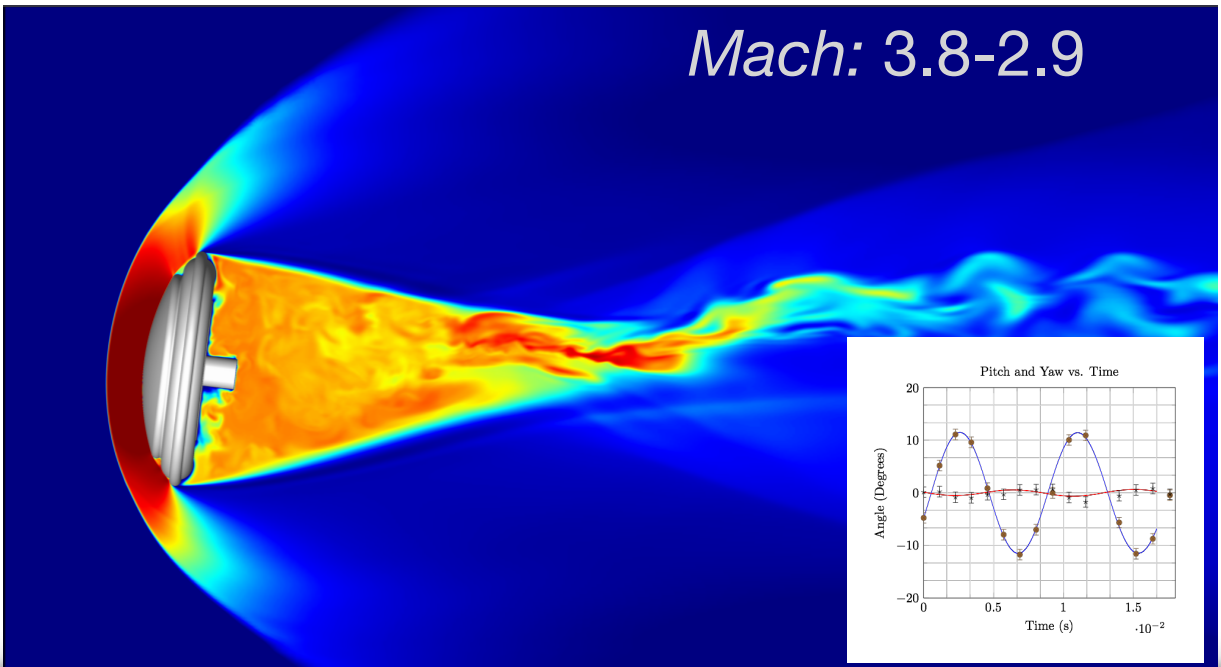
Utilities: Effective CMq curves, section fits

- Effective pitch damping integrated over one cycle
 - Map $C_{M_q}(\alpha) \rightarrow \bar{C}_{M_q}(\text{amplitude})$
 - C_{M_q} as a function of instantaneous α is required for integration into flight dynamics simulations
 - Effective C_{M_q} as a function of oscillation amplitude provides more intuitive insights about where the vehicle is stable and permits more readily digested comparisons between data-sets
 - With effective curve, limit cycle can be predicted for 1dof (simulation or experiment) and 3dof (flight-like) configurations
- Sectional fitting of effective CMq using analytical solutions
 - Shows good agreement with effective CMq curve computed above
 - Provides means to quantify scatter in curve

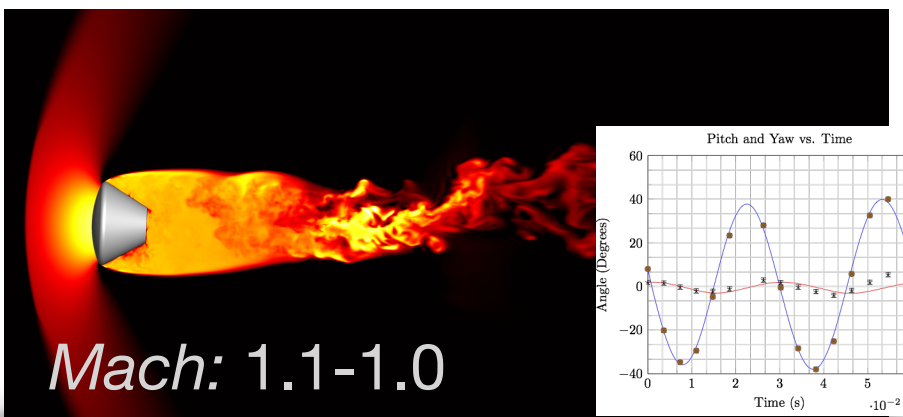
$$\bar{C}_{mq} = \frac{\int_0^{\frac{2\pi}{\omega}} (C_{mq} + C_{m\dot{\alpha}}) \dot{\alpha}^2 dt}{\int_0^{\frac{2\pi}{\omega}} \dot{\alpha}^2 dt}$$



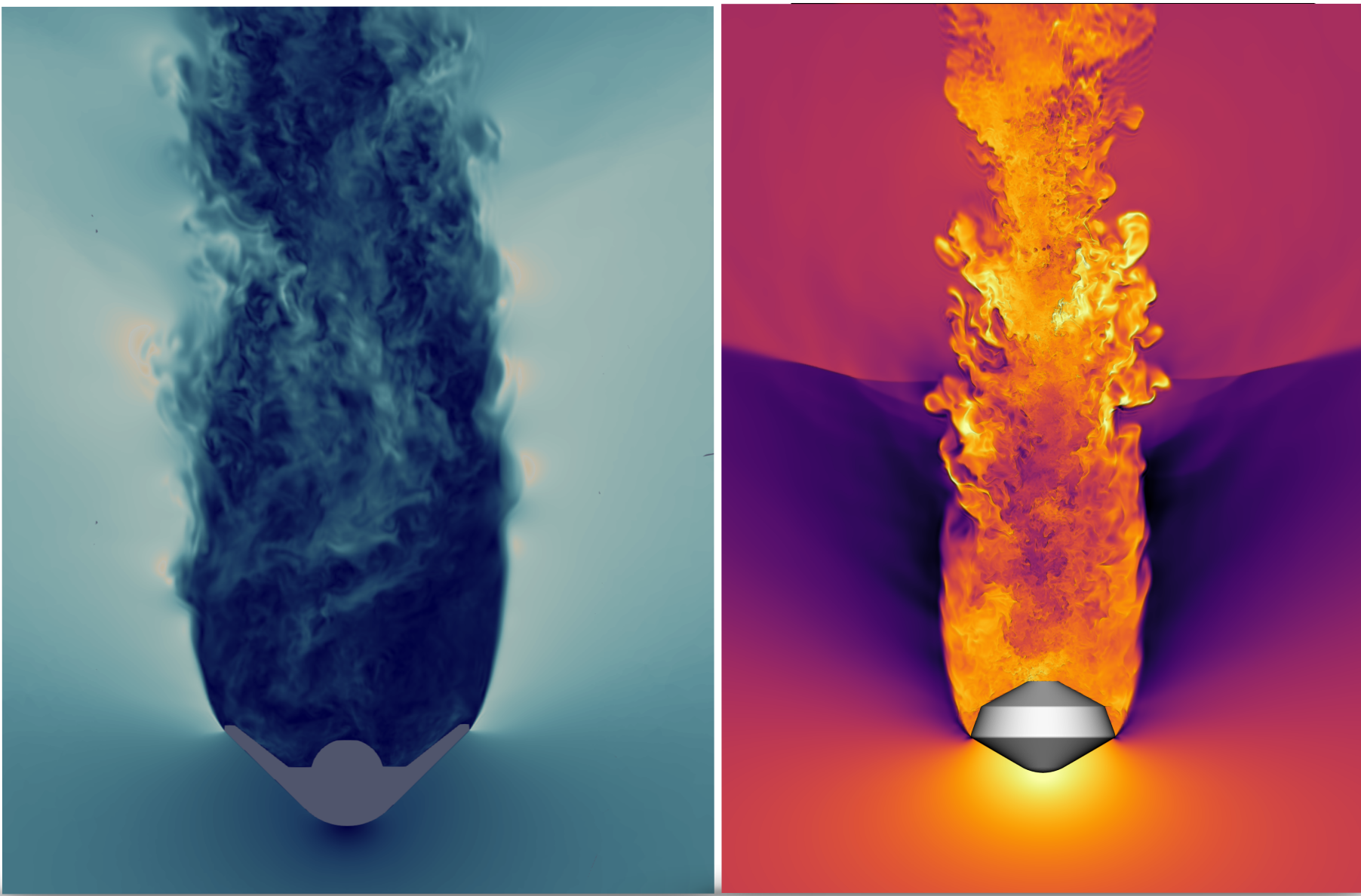
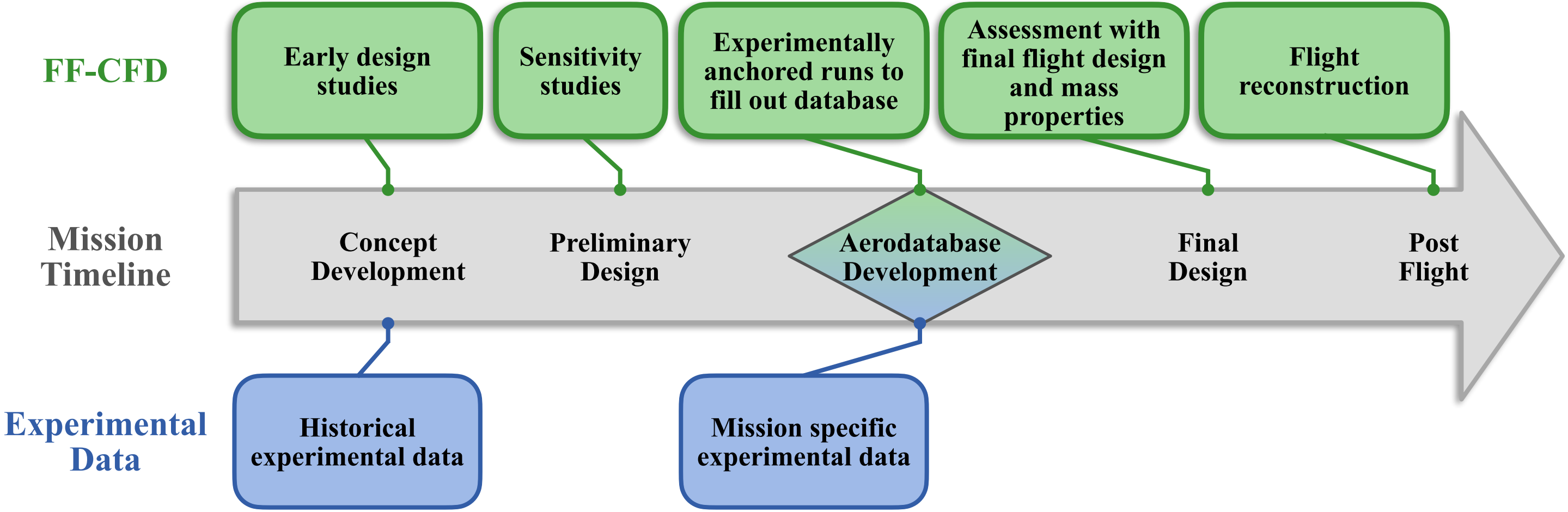
- ESM has invested in Free-Flight CFD capability to bring a computational tool into the portfolio for characterizing dynamic stability
- Extending CFD capability to quantify dynamic stability and perform sensitivity studies for flight projects requires verified and validated tools
 - FF-CFD in US3D has been extensively validated in the supersonic, transonic, and mid-subsonic regime
 - Dynamic simulations provide a new paradigm to simulate as you fly
- Effort in the last 18 months has expanded into developing the data reduction techniques necessary to produce full aerodynamic databases from FF-CFD data
- With a validated tool for modeling the dynamics and an established method for reducing data, computational tools can provide value throughout mission life



Mach: 2.4-1.2



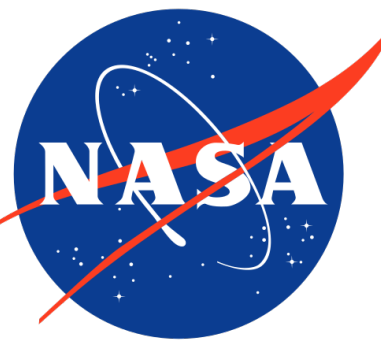
Mach: 1.1-1.0





Questions?

References



1. Stern, Eric, et al. "Dynamic CFD Simulations of the MEADS II Ballistic Range Test Model." AIAA Atmospheric Flight Mechanics Conference. 2016.
2. Brock, Joseph M., Eric C. Stern, and Michael C. Wilder. "Computational fluid dynamics simulations of supersonic inflatable aerodynamic decelerator ballistic range tests." Journal of Spacecraft and Rockets 56.2 (2019): 526-535.
3. Hergert, Jakob, et al. "Free-Flight Trajectory Simulation of the ADEPT Sounding Rocket Test Using US3D." *35th AIAA Applied Aerodynamics Conference*. 2017. Brown, Jeffrey D., et al. "Transonic Aerodynamics of a Lifting Orion Crew Capsule from Ballistic Range Data." Journal of Spacecraft and Rockets 47.1 (2010): 36-47.
4. Brock, Joseph M, et al. "Free-Flight CFD Simulations of Transonic MPCV Ballistic Range and Subsonic AA-2 Flight Test". Pending Journal of Spacecraft and Rockets submission
5. Schoenenberger, Mark, and Eric M. Queen. "Limit cycle analysis applied to the oscillations of decelerating blunt-body entry vehicles." NATO RTO Symposium AVT-152 on Limit-Cycle Oscillations and Other Amplitude-Limited, Self-Excited Vibrations. No. RTO-MP-AVT-152. 2008.
6. Stern, Eric, et al. "A Method for Deriving Capsule Pitch-Damping Coefficients from Free-Flight CFD Data". Pending Journal of Spacecraft and Rockets submission
7. McKown, Quincy E., et al. "Attitude Reconstruction of Free-Flight CFD Generated Trajectories Using Non-Linear Pitch Damping Coefficient Curves." AIAA SCITECH 2022 Forum. 2022.